

ADDENDUM NO. 1

2019 - Lobdell Lane over The Boquet River Bridge Replacement

Essex County, NY

August 12, 2019

TO ALL HOLDERS OF BIDDING DOCUMENTS:

This Addendum, issued to bid document holders of record, indicates clarifications to the bid documents for the *2019 Lobdell Lane over The Boquet River Bridge Replacement* project. All clarifications described herein shall be incorporated into the Contractor's bid proposal. This Addendum is part of the Contract Documents. Adjustments required by each item shall be understood to apply to all document references affected by the clarifications described.

1. **General:** A Pre-Bid meeting was held for the project at the sites on July 31, 2019 at 9:00 AM. Minutes from the meeting are enclosed and are a part of this Addendum and the Contract Documents.
2. **General:** A copy of the Geotechnical Report for the project is attached to this Addendum for reference only. This report is provided for informational purposes and shall not be considered to be part of the contract documents. If distributed to others by the bidder or contractor, they must be delivered in their entirety only.

It is the bidder's responsibility to determine if the information contained in these geotechnical reports is adequate for bidding purposes. The bidders may make their own investigations, tests and analyses for use in bid preparation if additional information is required. Contractors will not be relieved of any of their obligations for performance of the work for the project, nor shall they be entitled to any additional compensation on the premise of differing subsurface conditions or soils types which may be encountered.

Individual subsurface boring logs were prepared based upon the visual classifications and laboratory testing. The individual subsurface logs and keys explaining the terms used in their preparation are presented in the geotechnical reports and should be reviewed for a description of the conditions encountered at the specific test boring locations. It should be understood that conditions are only known at the specific depths and locations sampled. Conditions at other depths and locations may differ. Determinations of earthwork quantities for

bidding must not rely solely on the soil strata thicknesses measured at the discrete test boring locations completed for this investigation. The bidder should perform their own explorations as needed to obtain representative thicknesses of soil layers and strata as required to prepare their bids for the work.

3. **General:** There are no DBE/WBE/MBE goals for this project.
4. **Regarding Drawing N-1:** Replace with attached Drawing N-1, revision 1 - "Addendum No.1" dated 8/12/19.
5. **Regarding Drawing C-3:** Replace with attached Drawing C-3, revision 1 - "Addendum No.1" dated 8/12/19.
6. **Regarding Drawing C-3:** Replace with attached Drawing C-3, revision 1 - "Addendum No.1" dated 8/12/19.

END OF ADDENDUM NO. 1
(attachments)

Pre-Bid Meeting Minutes

PRE-BID MEETING MINUTES

Report Date: August 12, 2019

Project: Lobdell Lane over The Boquet River Bridge Replacement

Attending: Matthew Huntington, PE - Schoder Rivers Assoc.
Jim Dougan - Essex County DPW
Gary Rancour - Essex County DPW
Ed Shull- Rozell
Matt Schmitt - Bette & Cring
William Patenaude - Alpine Construction
Dane Insogna - Harrison & Burrowes
Richard Kondrat - Harrison & Burrowes
(Copy of attendance sheet is attached for information)

Distribution: Via posting on the Essex County Website as a part of Addendum No. 1 for access by all holders of bidding documents.

A scheduled pre-bid meeting was held for the above referenced project on July 31st at 9:00AM at the project site. The following items were discussed:

1. Huntington provided a general summary of the overall scope of work for the project and noted the geotechnical report will be included as part of Addendum No. 1.
2. Patenaude noted the location of a Gravel Pit at the southern end of Lobdell Lane and inquired if that material is available for use during construction of the project. Rancour stated that the pit is privately owned and to the best of his knowledge is not currently active.
3. Rancour noted that excess non-hazardous construction and demolition debris may disposed of at the Essex County DPW Highway yard.
4. Huntington noted that the maximum design loading for the existing temporary bridge is AASHTO HS-20.

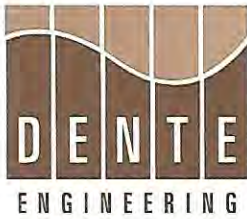
The meeting adjourned at 9:30 AM.

Respectfully submitted:



Matthew Huntington, PE
Sr. Project Engineer

Geotechnical Report



ALBANY AREA

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Watervliet, NY 12189
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Fax 518-266-9238

BUFFALO AREA

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Orchard Park, NY 14127
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Fax 716-648-3521

May 16, 2016

Mr. Jim Dougan
Essex County DPW
8053 Route 9
Elizabethtown, NY 12932

Re: Geotechnical Study
Lobdell Lane Bridge over Boquet River
Elizabethtown, NY
Project Number No. FDE-15-280

Gentlemen;

In accord with your authorization, we have completed a subsurface investigation and prepared this geotechnical evaluation report for the planned replacement of a bridge carrying Lobdell Lane over the Boquet River in Elizabethtown, New York.

This report presents the results of the subsurface investigation completed at the site on May 4, a summary of the conditions disclosed, and our recommendations for the design and construction of the geotechnical aspects of the project.

Subsurface Conditions

The Subsurface Investigation completed at the site consisted of two (2) exploratory test borings, one at each side of the planned bridge abutments. The borings were performed where accessible and without utility conflicts in the general vicinity of the locations shown on the attached Subsurface Investigation Plan. The bores were advanced using a rotary drill rig mounted on a trailer, and overburden soils were sampled in general accord with the procedures of ASTM D-1586. Subsurface Logs were prepared and are attached to this report, together with sheets that explain the terms used in their preparation. It should be understood that boring logs present a description of the conditions encountered on the date, specific locations investigated, and to the depths sampled. Conditions at locations and depths other than those investigated may differ. It should also be understood that conditions can change with time.

The Subsurface Logs should be reviewed for the specific conditions encountered at each investigated location. The borings were advanced from the previous roadway grades at the site and, as such, penetrated soil fill, which is believed to have been placed to establish the grades for the approach roads to the former bridge crossing.

The fill soils were composed of a mixture of sand, silt, and gravel with lesser amounts of cobbles. These fills were moist throughout and judged to be of a loose to firm relative density. The fills extended to estimated depths of between about 12 and 13 feet.

Underlying the fill soils are glacial outwash soils composed of alternating strata of fine sand and silt throughout the depths explored at location B-2. These soils were of a generally loose to firm relative density and extended to depths of about 49 feet at location B-1 where they graded into a medium consistency silt and clay deposit which extended through the depths explored, about 52 feet.

Groundwater did not accumulate within the augers prior to the introduction of drilling fluid/water and thus was not measured within the test borings advanced at the site. In our opinion, these measurements are not representative of the true saturated ground level at the time of the study. Groundwater should be expected to coincide with the river level at the site throughout the seasons.

Geotechnical Recommendations

In our opinion the planned bridge may be supported upon spread foundations within sheet piles installed for scour protection, if required. It should be understood that if the spread foundation option is selected, all fills and any organic materials contained within or beneath these fill soils must be removed from beneath the foundations.

Based on the available subsurface information Seismic Site Class D should be used. The soils, during the design seismic event, should not liquify.

Steel sheet piles may be used to form a cofferdam or an abutment wall, both designed as a cantilever or tied back system. If steel sheetpiling is used, it will be necessary to remove obstructions as the fills and native soils may contain cobbles and boulders in areas.

Excavation to establish bearing for foundations should proceed through the fill and any buried organic soils, or at least one (1) foot beneath these grades, whichever is deeper. Structural fill required to establish the design bearing grade should extend beyond the edge of the foundations a distance at least equal to half the depth of the structural fill placed beneath the foundations. The bearing grade excavation should be backfilled with a run of crusher-run stone similar in gradation and quality to a NYSDOT Section 304 Type 2 Material. The material should be placed in a single lift and be compacted to at least 95 percent of its maximum dry density established through the procedures of ASTM D-1557, the Modified Proctor Test.

If the grades are established at or within a foot of the river/groundwater levels, we recommend the foundation grade be prepared by placing a layer of synthetic fabric

such as Mirafi 500X upon the approved bearing grade, followed by at least 12 inches of a 50/50 blend of NYSDOT number 1 and 2 sized aggregate to create a working surface that can also be dewatered with ordinary sumps and pumps set within it.

Dependent upon river levels during construction, the excavations planned may penetrate saturated soils and groundwater, which will coincide with the river levels in the immediate project area. Common sump and pump techniques from within cofferdam sheets and behind sheetpile walls should be capable of limited depression and control of the water table at this site. The dewatering system must be designed and operated to assure that the system does not fail and allow groundwater to rise, possibly creating "quick" conditions at the bearing grades within the cofferdam or buoyant forces upon partially completed structures.

Sheet pile cantilever walls or enclosed cofferdams should be designed to achieve stability for varying water elevations that might occur during the construction process. The Contractor's dewatering plan, as well as any construction sheeting and shoring, should be designed by a Licensed Professional Engineer. The design should meet the requirements of 29 CFR Part 1926 Occupational Safety and Health Standards - Excavations for Type C Soils.

The structural fill used to backfill the abutment walls above the water table should consist of NYSDOT Section 304 Type 4 Processed Sand and Gravel material. The fill should be placed in loose layers no more than one (1) foot thick and each layer be compacted to no less than 95 percent of the material's maximum dry density determined through the procedures of ASTM D-1557, the Modified Proctor Compaction test.

The following parameters are recommended for use in the design of the bridge foundations, abutments, and wing walls;

Fill Parameters

- | | | | |
|----|--|---|-----------------|
| 1. | Overburden Unit Weight (Total) | = | 125 lbs/Cu. Ft. |
| 2. | Friction Angle of Soil | = | 30 Degrees |
| 3. | Coefficient of Active Earth pressure | = | 0.33 |
| 4. | Coefficient of At-Rest Earth pressure | = | 0.5 |
| 5. | Coefficient of Passive Earth pressure | = | 3.0 |
| 6. | Coefficient of Sliding Friction | = | 0.58 |
| 7. | Resistance Factor for Passive Resistance | = | 0.50 |
| 8. | Resistance Factor for Shear Resistance | = | 0.80 |

Sand/Gravel/Silt Overburden Parameters

- | | | | |
|----|---------------------------------------|---|-----------------|
| 1. | Factored Bearing Resistance | = | 3,500 PSF |
| 2. | Nominal Bearing Resistance | = | 10,500 PSF |
| 3. | Overburden Unit Weight (Total) | = | 135 lbs/Cu. Ft. |
| 4. | Friction Angle of Soil | = | 32 Degrees |
| 5. | Coefficient of Active Earth pressure | = | 0.31 |
| 6. | Coefficient of At-Rest Earth pressure | = | 0.47 |
| 7. | Coefficient of Passive Earth pressure | = | 3.25 |

8. Coefficient of Sliding Friction = 0.58
9. Resistance Factor for Passive Resistance = 0.50
10. Resistance Factor for Shear Resistance = 0.80

Abutment and sheet pile abutment walls should be designed to restrain lateral earth pressures calculated for the At-Rest Condition. Wing and temporary cofferdams may be designed to resist Active Lateral Earth Pressures.

Settlement of the bridge's spread foundations should occur in a semi-elastic manner as loads are actually applied and cease with each incremental loading of the foundations. We believe that the foundations will settle in total and differentially less than about one (1) and one-half (½) inches, respectively, provided our recommendations concerning bearing grade preparation are followed. It should be understood that actual settlements will be dependent in great part upon the care exercised during bearing grade preparation.

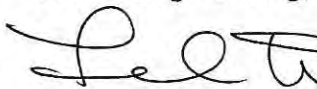
Summary

This report was prepared for specific application to the project site and the construction planned. It was prepared on the basis of a limited number of investigated locations at the site. Subsurface conditions at other than the investigated locations may be different. We should be allowed the opportunity to review appropriate plans and specifications prior to their release for bidding. The Geotechnical Engineer should be retained to observe and test earthwork and bearing grades during construction. This report was prepared using methods and practices common to Geotechnical Engineering in the area and at the time. No other warranties, expressed or implied, are made.

A sheet entitled "Important Information about your Geotechnical Engineering Report" prepared by the Association of Engineering Firms Practicing in the Geosciences is attached to this report. This sheet should never be separated from this report and be carefully reviewed as it sets the only context within which this report should be used.

We appreciate the opportunity to be of service. Should questions arise or if we may be of any other service, please contact us at your convenience.

Yours truly,
Dente Engineering, P.C.



Fred A. Dente, P.E.
President



Enclosures;

Important Information about This

Geotechnical-Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical-engineering study conducted for a civil engineer may not fulfill the needs of a constructor — a construction contractor — or even another civil engineer. Because each geotechnical-engineering study is unique, each geotechnical-engineering report is unique, prepared *solely* for the client. No one except you should rely on this geotechnical-engineering report without first conferring with the geotechnical engineer who prepared it. *And no one — not even you — should apply this report for any purpose or project except the one originally contemplated.*

Read the Full Report

Serious problems have occurred because those relying on a geotechnical-engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

Geotechnical Engineers Base Each Report on a Unique Set of Project-Specific Factors

Geotechnical engineers consider many unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk-management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical-engineering report that was:

- not prepared for you;
- not prepared for your project;
- not prepared for the specific site explored; or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical-engineering report include those that affect:

- the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a light-industrial plant to a refrigerated warehouse;
- the elevation, configuration, location, orientation, or weight of the proposed structure;
- the composition of the design team; or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project changes—even minor ones—and request an

assessment of their impact. *Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.*

Subsurface Conditions Can Change

A geotechnical-engineering report is based on conditions that existed at the time the geotechnical engineer performed the study. *Do not rely on a geotechnical-engineering report whose adequacy may have been affected by:* the passage of time; man-made events, such as construction on or adjacent to the site; or natural events, such as floods, droughts, earthquakes, or groundwater fluctuations. *Contact the geotechnical engineer before applying this report to determine if it is still reliable.* A minor amount of additional testing or analysis could prevent major problems.

Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ — sometimes significantly — from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide geotechnical-construction observation is the most effective method of managing the risks associated with unanticipated conditions.

A Report's Recommendations Are Not Final

Do not overrely on the confirmation-dependent recommendations included in your report. *Confirmation-dependent recommendations are not final*, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations *only* by observing actual subsurface conditions revealed during construction. *The geotechnical engineer who developed your report cannot assume responsibility or liability for the report's confirmation-dependent recommendations if that engineer does not perform the geotechnical-construction observation required to confirm the recommendations' applicability.*

A Geotechnical-Engineering Report Is Subject to Misinterpretation

Other design-team members' misinterpretation of geotechnical-engineering reports has resulted in costly

problems. Confront that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Constructors can also misinterpret a geotechnical-engineering report. Confront that risk by having your geotechnical engineer participate in prebid and preconstruction conferences, and by providing geotechnical construction observation.

Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical-engineering report should *never* be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, *but recognize that separating logs from the report can elevate risk.*

Give Constructors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make constructors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give constructors the complete geotechnical-engineering report, *but* preface it with a clearly written letter of transmittal. In that letter, advise constructors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. *Be sure constructors have sufficient time* to perform additional study. Only then might you be in a position to give constructors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

Read Responsibility Provisions Closely

Some clients, design professionals, and constructors fail to recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations," many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help

others recognize their own responsibilities and risks. *Read these provisions closely.* Ask questions. Your geotechnical engineer should respond fully and frankly.

Environmental Concerns Are Not Covered

The equipment, techniques, and personnel used to perform an *environmental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnical-engineering report does not usually relate any environmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures.* If you have not yet obtained your own environmental information, ask your geotechnical consultant for risk-management guidance. *Do not rely on an environmental report prepared for someone else.*

Obtain Professional Assistance To Deal with Mold

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the *express purpose* of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold-prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, many mold-prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical-engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; *none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.*

Rely, on Your GBC-Member Geotechnical Engineer for Additional Assistance

Membership in the Geotechnical Business Council of the Geoprofessional Business Association exposes geotechnical engineers to a wide array of risk-confrontation techniques that can be of genuine benefit for everyone involved with a construction project. Confer with your GBC-Member geotechnical engineer for more information.

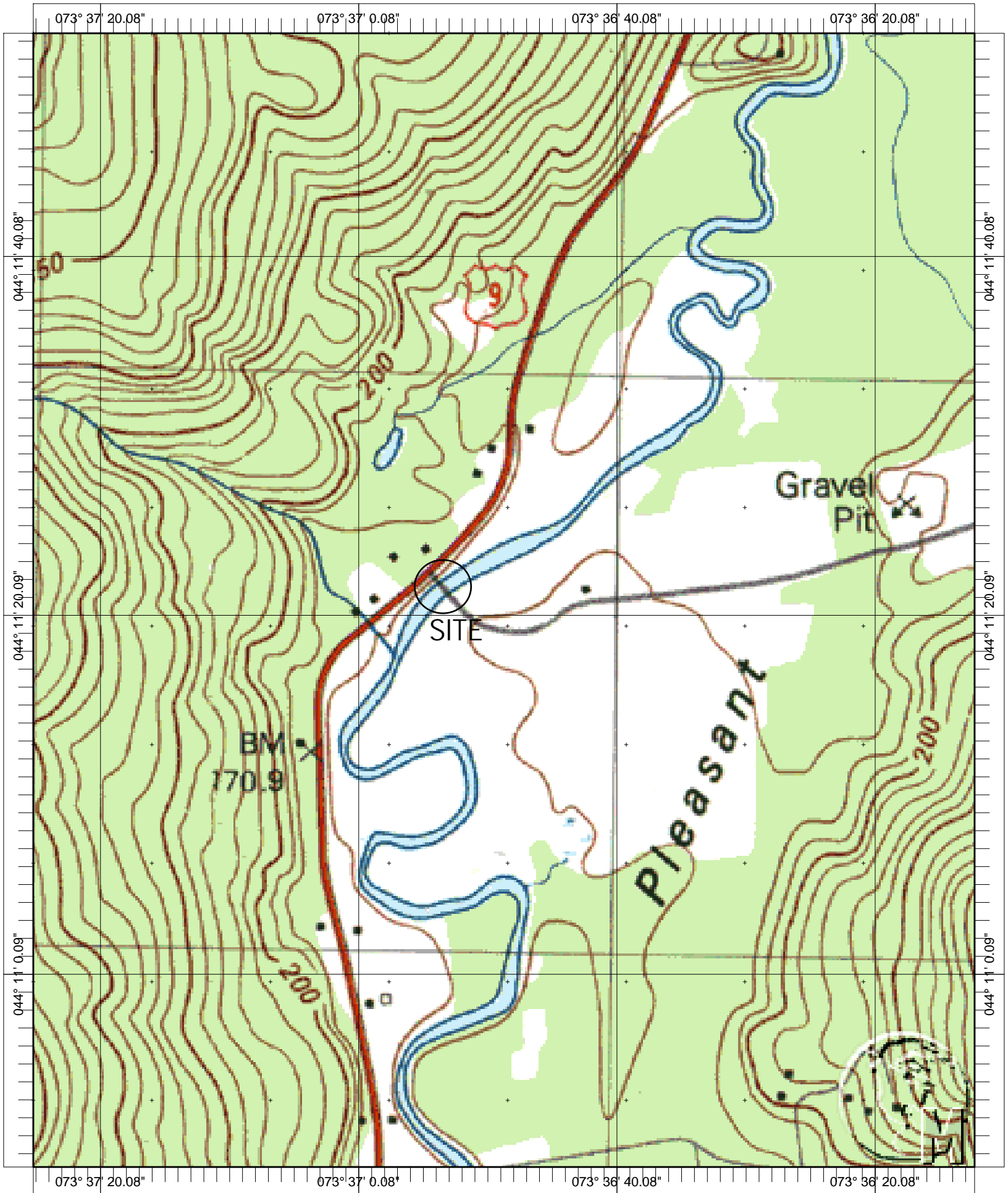


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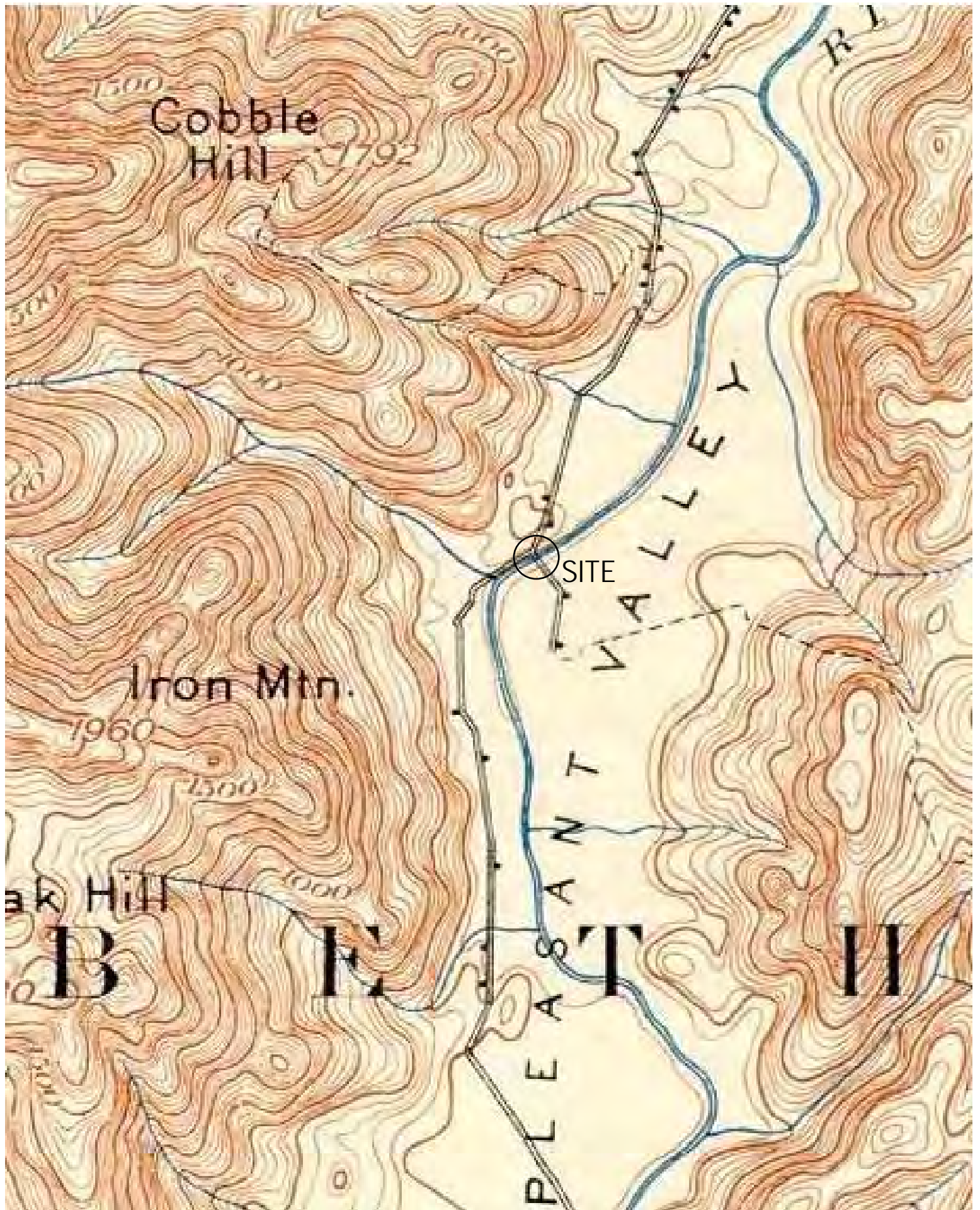
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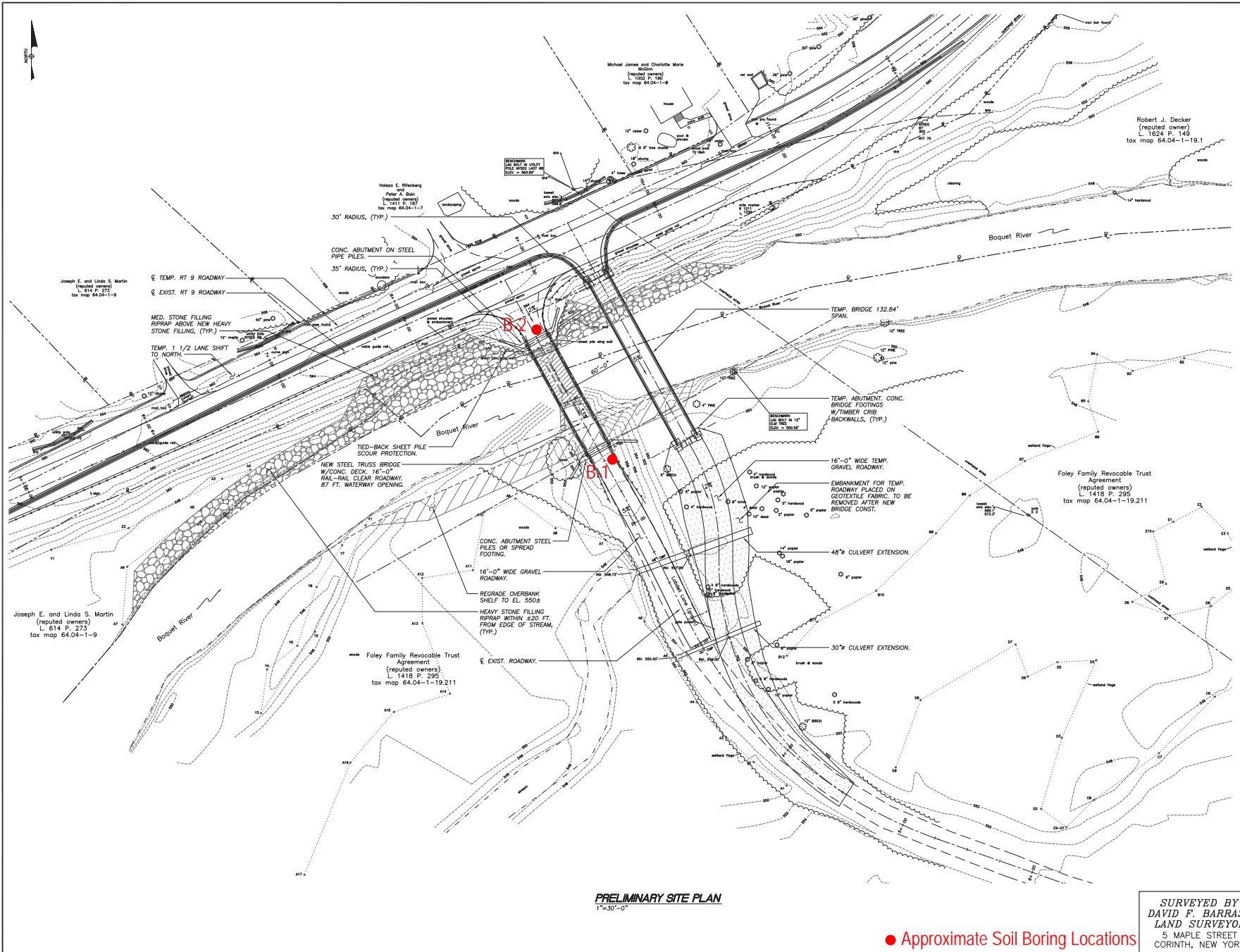


Name: ELIZABETHTOWN
Date: 5/10/116
Scale: 1 inch equals 666 feet

Location: 044° 11' 20.9" N 073° 36' 48.9" W
Caption: LOBDELL LANE BRIDGE
ELIZABETHTOWN, NY
FDE-15-280



Lobbell Lane Bridge, Elizabethtown, New York 1901



NOTE: TEMPORARY ROADWAY (ROUTE 9) ALIGNMENT SHALL REVERT TO EXISTING ALIGNMENT AND TRAFFIC FLOW CONDITIONS UPON COMPLETION OF THE BRIDGE REPLACEMENT WORK AND REESTABLISHMENT OF LOBDELL LANE ROADWAY.

NOTE: SEE DRAWING DOT-2 FOR DETAIL ON TEMPORARY LANE SHEET.

LEGEND

- 550--- EXIST. CONTOUR
- EXIST. OVERHEAD UTILITY
- EXIST. EDGE OF STREAM
- CONSTRUCTION BASELINE
- TREE LINE

REV.	DATE	DESCRIPTION
0	1/11/16	ISSUED FOR REVIEW

**PRELIMINARY
NOT FOR
CONSTRUCTION**

UNAUTHORIZED ALTERATION OR ADDITION TO THIS DOCUMENT IS A VIOLATION OF SECTION 7208 SUBDIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

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 Evergreen Professional Park
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 (518) 781-0417, FAX: (518) 781-0513

SCALE: 1"=30'-0" DRAWN BY: SRA
 DATE: 1/11/16 ENG. BY: CBS
 PROJ. NO: 12-474.15 CHK'D BY: CBS

CLIENT NAME:
**ESSEX COUNTY DEPARTMENT
 OF PUBLIC WORKS
 Elizabethtown, N.Y.**

DRAWING TITLE:
**LOBDELL LANE BRIDGE
 OVER BOQUET RIVER
 REPLACEMENT**

PRELIMINARY SITE PLAN
 DRAWING NO. **P-1** SHT. 1 OF 2
 REV. 0

PRELIMINARY SITE PLAN
 1"=30'-0"

● Approximate Soil Boring Locations

**SURVEYED BY
 DAVID F. BARRASS
 LAND SURVEYOR**
 5 MAPLE STREET
 CORINTH, NEW YORK

INTERPRETATION OF SUBSURFACE LOGS

The Subsurface Logs present observations and the results of tests performed in the field by the Driller, Technicians, Geologists and Geotechnical Engineers as noted. Soil/Rock Classifications are made visually, unless otherwise noted, on a portion of the materials recovered through the sampling process and may not necessarily be representative of the materials between sampling intervals or locations.

The following defines some of the terms utilized in the preparation of the Subsurface Logs.

SOIL CLASSIFICATIONS

Soil Classifications are visual descriptions on the basis of the Unified Soil Classification ASTM D-2487 and USBR, 1973 with additional comments by weight of constituents by BUHRMASTER. The soil density or consistency is based on the penetration resistance determined by ASTM METHOD D1586. Soil Moisture of the recovered materials is described as DRY, MOIST, WET or SATURATED.

SIZE DESCRIPTION		RELATIVE DENSITY/CONSISTENCY (basis ASTM D1586)			
SOIL TYPE	PARTICLE SIZE	GRANULAR SOIL		COHESIVE SOIL	
BOULDER	> 12	DENSITY	BLOWS/FT.	CONSISTENCY	BLOWS/FT.
COBBLE	3" - 12"	LOOSE	< 10	VERY SOFT	< 3
GRAVEL-COARSE	3" - 3/4"	FIRM	11 - 30	SOFT	4 - 5
GRAVEL - FINE	3/4" - #4	COMPACT	31 - 50	MEDIUM	6 - 15
SAND - COARSE	#4 - #10	VERY COMPACT	50 +	STIFF	16 - 25
SAND - MEDIUM	#10 - #40			HARD	25 +
SAND - FINE	#40 - #200				
SILT/NONPLASTIC	< #200				
CLAY/PLASTIC	< #200				

SOIL STRUCTURE		RELATIVE PROPORTION OF SOIL TYPES	
STRUCTURE	DESCRIPTION	DESCRIPTION	% OF SAMPLE BY WEIGHT
LAYER	6" THICK OR GREATER	AND	35 - 50
SEAM	6" THICK OR LESS	SOME	20 - 35
PARTING	LESS THAN 1/4" THICK	LITTLE	10 - 20
VARVED	UNIFORM HORIZONTAL PARTINGS OR SEAMS	TRACE	LESS THAN 10

Note that the classification of soils or soil like materials is subject to the limitations imposed by the size of the sampler, the size of the sample and its degree of disturbance and moisture.

ROCK CLASSIFICATIONS

Rock Classifications are visual descriptions on the basis of the Driller's, Technician's, Geologist's or Geotechnical Engineer's observations of the coring activity and the recovered samples applying the following classifications.

CLASSIFICATION TERM	DESCRIPTION
VERY HARD	NOT SCRATCHED BY KNIFE
HARD	SCRATCHED WITH DIFFICULTY
MEDIUM HARD	SCRATCHED EASILY
SOFT	SCRATCHED WITH FINGERNAIL
VERY WEATHERED	DISINTEGRATED WITH NUMEROUS SOIL SEAM
WEATHERED	SLIGHT DISINTEGRATION, STAINING, NO SEAMS
SOUND	NO EVIDENCE OF ABOVE
MASSIVE	ROCK LAYER GREATER THAN 36" THICK
THICK BEDDED	ROCK LAYER 12" - 36"
BEDDED	ROCK LAYER 4" - 12"
THIN BEDDED	ROCK LAYER 1" - 4"
LAMINATED	ROCK LAYER LESS THAN 1"
FRACTURES	NATURAL BREAKS AT SOME ANGLE TO BEDS

Core sample recovery is expressed as percent recovered of total sampled. The ROCK QUALITY DESIGNATION (RQD) is the total length of core sample pieces exceeding 4" length divided by the total core sample length for N size cored.

GENERAL

- Soil and Rock classifications are made visually on samples recovered. The presence of Gravel, Cobbles and Boulders will influence sample recovery classification density/consistency determination.
- Groundwater, if encountered, was measured and its depth recorded at the time and under the conditions as noted.
- Topsoil or pavements, if present, were measured and recorded at the time and under the conditions as noted.
- Stratification Lines are approximate boundaries between soil types. These transitions may be gradual or distinct and are approximated.

DENTE ENGINEERING, P.C.

SUBSURFACE LOG B-1

PROJECT: Lobdell Lane Bridge

DATE

START: 5/4/16

FINISH: 5/4/16

LOCATION: Essex County DPW

METHODS: 3 1/4" Hollow Stem Augers, ASTM

CLIENT: Essex County DPW

D1586 Drilling Methods with Auto Hammer

JOB NUMBER: FDE-15-280

SURFACE ELEVATION: +/- 560.0'

DRILL TYPE: CME 45C

CLASSIFICATION: O.Burns

SAMPLE		BLOWS ON SAMPLER					CLASSIFICATION / OBSERVATIONS
DEPTH	#	6"	12"	18"	24"	N	
5'	1	1	2				FILL: Brown/Gray F-C SAND and GRAVEL, trace silt (MOIST) Grades Brown F-C SAND, Little Gravel, trace silt Grades Some Gravel
				3	2	5	
	2	4	4				
				6	7	10	
	3	3	4				
10'				2	3	6	Similar with rootlets noted Grades to Brown/Gray, Little Gravel
	4	6	2				
				2	1	4	
	5	2	1				
				1	1	2	
15'	6	2	1				Grades Dark Brown F-M SAND, Little Coarse Sand and Gravel (MOIST, LOOSE) Dark Brown Fine SAND and SILT (MOIST, LOOSE) Brown F-M SAND, Little Silt and Mottling (WET) (WET, LOOSE)
				1	2	2	
	7	1	1				
				2	4	3	
	8	2	1/18"				
20'		1/12"	-				Brown/Orange GRAVEL, Some F-C Sand, trace silt (WET, LOOSE TO FIRM)
				3	18	3	
	10	12	14				
				14	8	28	
25'							Gray Fine SAND, Some Silt (SATURATED)
	11	2	4				
				3	3	7	
30'							

DENTE ENGINEERING, P.C.

SUBSURFACE LOG B-1 contin.

PROJECT: Lobdell Lane Bridge

DATE

START: 5/4/16

FINISH: 5/4/16

LOCATION: Essex County DPW

METHODS: 3 1/4" Hollow Stem Augers, ASTM

CLIENT: Essex County DPW

D1586 Drilling Methods with Auto Hammer

JOB NUMBER: FDE-15-280

SURFACE ELEVATION: +/- 560.0'

DRILL TYPE: CME 45C

CLASSIFICATION: O.Burns

SAMPLE		BLOWS ON SAMPLER					CLASSIFICATION / OBSERVATIONS
DEPTH	#	6"	12"	18"	24"	N	
	12	1	1				Gray Fine SAND, Some Silt (SATURATED, FIRM TO LOOSE)
				2	1	3	
35'	13	1	1				Brown/Gray Varved SILT with F-M Sand and Clay Partings
				2	10	3	
40'	14	4	6				Similar with Fine Sand Seams
				8	9	14	
45'	15	5	7				(SATURATED, LOOSE TO FIRM)
				7	8	14	
50'	16	5	5				Brown/Gray SILT and CLAY (SATURATED, MEDIUM)
				8	10	13	
55'							End of boring 52.0' depth.
60'							

DENTE ENGINEERING, P.C.

SUBSURFACE LOG B-2

PROJECT: Lobdell Lane Bridge

DATE

START: 5/4/16

FINISH: 5/4/16

LOCATION: Essex County DPW

METHODS: 3 1/4" Hollow Stem Augers, ASTM

CLIENT: Essex County DPW

D1586 Drilling Methods with Auto Hammer

JOB NUMBER: FDE-15-280

SURFACE ELEVATION: +/- 564.0'

DRILL TYPE: CME 45C

CLASSIFICATION: O.Burns

SAMPLE		BLOWS ON SAMPLER					CLASSIFICATION / OBSERVATIONS
DEPTH	#	6"	12"	18"	24"	N	
5'	1	13	18				FILL: Brown/Gray F-C SAND and GRAVEL, trace silt (MOIST) Grades trace plastic
				15	10	33	
	2	7	7				
				7	22	14	
	3	9	13				
10'				8	6	21	Grades Little Asphalt Grades Brown Mottled F-M SAND, Some Gravel, Little Coarse Sand and Silt (MOIST, COMPACT TO LOOSE)
	4	8	7				
				6	6	13	
	5	9	6				
				5	3	11	
15'	6	2	3				Brown F-C SAND and GRAVEL, trace silt (MOIST, LOOSE) Brown Fine SAND, Little Silt
				4	3	7	
	7	2	3				
				4	3	7	
20'	8	3	5				(SATURATED, FIRM) Brown/Gray Banded Fine SAND and SILT
				7	10	12	
	9	1	1				
				1	3	2	
25'							(SATURATED, LOOSE) Brown/Gray Fine SAND, Some Silt
	10	3	4				
				6	6	10	
30'						(SATURATED, LOOSE)	

DENTE ENGINEERING, P.C.

SUBSURFACE LOG B-2 contin.

PROJECT: Lobdell Lane Bridge

DATE

START: 5/4/16

FINISH: 5/4/16

LOCATION: Essex County DPW

METHODS: 3 1/4" Hollow Stem Augers, ASTM

CLIENT: Essex County DPW

D1586 Drilling Methods with Auto Hammer

JOB NUMBER: FDE-15-280

SURFACE ELEVATION: +/- 564.0'

DRILL TYPE: CME 45C

CLASSIFICATION: O.Burns

SAMPLE		BLOWS ON SAMPLER					CLASSIFICATION / OBSERVATIONS
DEPTH	#	6"	12"	18"	24"	N	
35'	11	1	2				Gray SILT and Fine SAND
				1	2	3	
40'	12	1	1				
				2	4	3	
45'	13	1	2				(SATURATED, LOOSE)
				3	3	5	
50'	14	7	9				Brown/Gray SILT with Occasional F-M Sand and Clay Partings
				10	11	19	
55'	15	6	7				(SATURATED, FIRM)
				9	9	16	
60'							End of boring 52.0' depth.

View northwest toward the area of B-1



View southeast across the bridge from the area of B-2





April 17, 2018

Mr. Jim Dougan
Essex County DPW
8053 Route 9
Elizabethtown, NY 12932

Re: Supplemental Geotechnical Evaluation
Lobdell Lane Bridge over Boquet River
Elizabethtown, New York
Dente File No. JB175555

Mr. Dougan,

Presented herein are the results of a supplemental subsurface investigation and geotechnical evaluation we completed to assist in planning for replacement of the Lobdell Lane bridge over the Boquet River in Elizabethtown, New York. Our services were provided in general accordance with our proposal dated September 14, 2017 which was accepted by the County.

In May 2016 we submitted our original Geotechnical Study for this project which recommended supporting the new bridge on spread foundations with sheet piles installed as needed for scour protection. These recommendations were based upon the results of two test borings taken to a depth of about 50 feet. To expand upon our original recommendations and evaluate whether pile support is an option, we extended the borings and evaluated various options for the foundation design with the project engineer, Schoder Rivers Associates (SRA).

SUBSURFACE PROFILE

In February 2018 we extended the original test borings to depths of about 102 feet. A plan showing the approximate boring locations and logs prepared by a Geotechnical Engineer are attached.

Dente Group, A Terracon Company 594 Broadway Watervliet, NY 12189
P (518) 266-0310 F (518) 266-9238 terracon.com

Environmental



Facilities



Geotechnical



Materials

As detailed in our original report, the test borings first encountered granular embankment fills which extended to depths of about 12 to 15 feet below the road surface. The fills were underlain by glacial outwash soils composed of fine sand and silt mixtures of loose to firm relative density. At depths of about 35 to 50 feet below the road surface, the glacial outwash soils graded to variable mixtures of silt or clayey silt with lesser amount of sand. These soils were judged to be of a loose to firm relative density or very soft to medium consistency and they extended to the maximum 102 foot depths explored.

CONCLUSIONS AND RECOMMENDATIONS

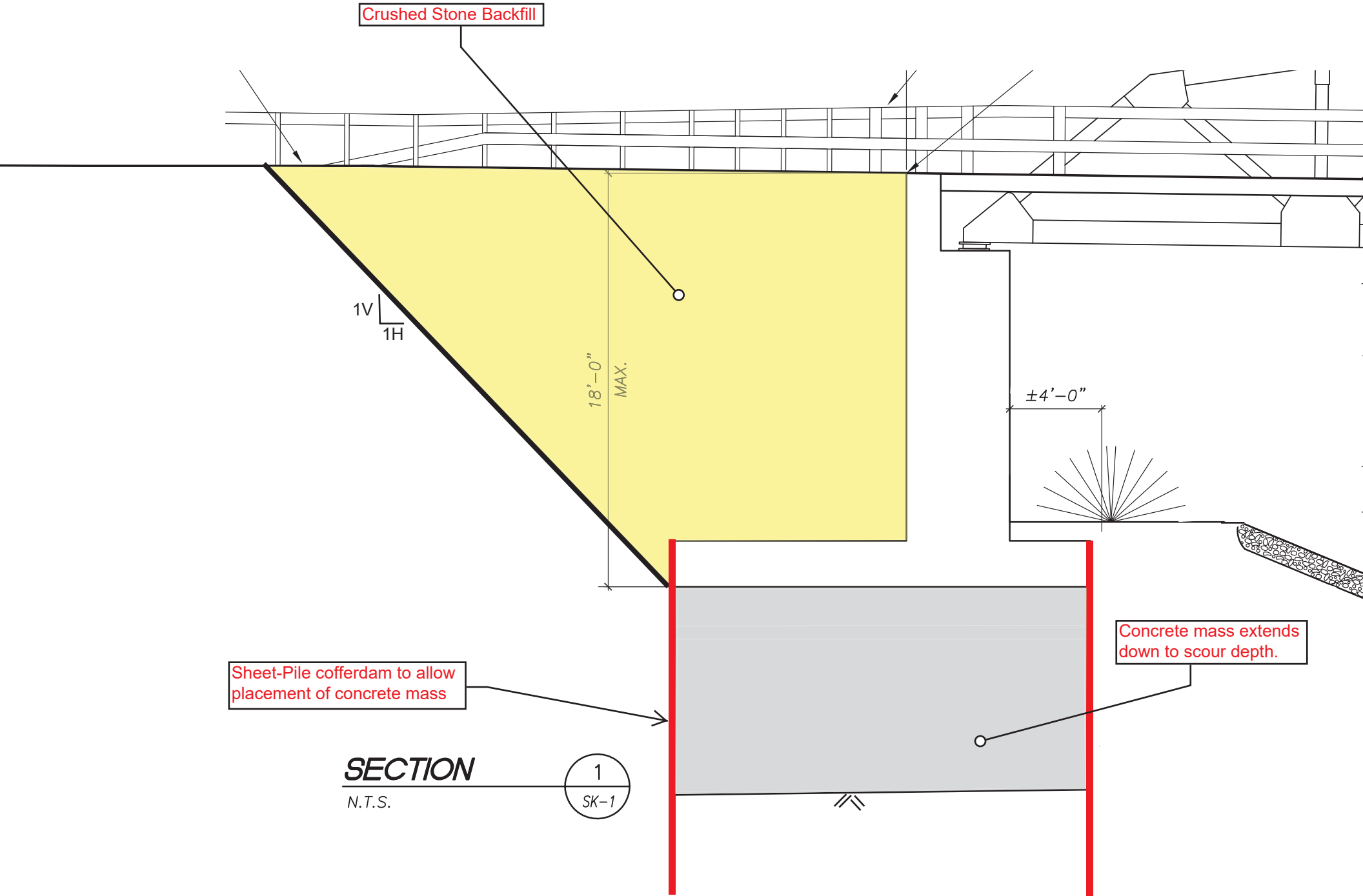
It is our opinion that the soils encountered within a depth of about 102 feet below the road surface are not a suitable bearing stratum to support a deep pile foundation system for the bridge. The allowable capacity for either a typical friction or end bearing pile in these soils would be inadequate to support the expected loads. On this basis, we continue to recommend that the bridge be supported on a shallow spread foundation system, with appropriate scour protection provided.

SRA has indicated to us that the south abutment can be designed using the recommendations contained in our original report. However, to reduce the height of the north abutment to within a tolerable limit for a standard cantilever wall design, the foundation must be seated no deeper than elevation 545.7 feet. This bearing elevation is about 4.4 feet above the scour depth estimated by SRA.

Various alternatives to provide the required scour protection were evaluated with SRA including options to provide a sheet-pile system in front of the abutment along with potential use of light-weight aggregate or geofam as backfill, or providing anchorage for the abutment and/or the sheet-piles. Based upon this evaluation, the option shown on the following sketch was deemed feasible and we understand will be implemented by SRA in their design. As shown, this option entails constructing the abutment foundation on a base of mass concrete placed within a sheet-pile cofferdam and backfilling the abutment placed upon it with clean crushed stone to reduce lateral loads on the abutment.

The concrete infill within the sheet-pile cofferdam should be taken to or below the expected scour depth. The concrete may be tremied in place immediately as the excavation is completed and it should have a minimum 28-day compressive strength equal to 2500 psi. The sheets should be designed by the contractor's engineer for the short-term conditions as the excavation is made and backfilled with concrete. For sheet-pile design purposes, the fine sand and silt soils can be assumed to have a total unit weight equal to 118 pcf and friction angle equal to 30 degrees.

Assuming that the abutment is backfilled with clean crushed stone composed of ASTM C33 Blend 57 aggregate, the lateral earth pressures and surcharge loads acting on the wall can be determined assuming:



Crushed Stone Backfill

1V
1H

18'-0"
MAX.

±4'-0"

Sheet-Pile cofferdam to allow placement of concrete mass

Concrete mass extends down to scour depth.

SECTION

N.T.S.

1
SK-1



CRUSHED STONE DESIGN PARAMETERS

- Total Unit Weight of Crushed Stone = 100 pcf
- Friction Angle of Crushed Stone = 40 degrees
- Coefficient of Active Earth Pressure = 0.22
- Coefficient of At-Rest Earth Pressure = 0.36

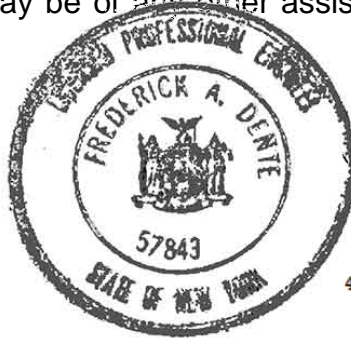
For design of the foundations, a coefficient of sliding friction equal to 0.70 can be assumed along with a factored bearing resistance equal to 3500 psf. Settlement of the foundation should be less than one inch. Most of this settlement should occur quickly as the bridge is constructed and loads are applied.

We appreciate the opportunity to provide these supplemental services. Should questions arise or if we may be of any other assistance, please contact us at your convenience.

Prepared by,
Dente Group

Edward Gravelle

Edward C. Gravelle, P.E.
Senior Engineer



4/17/18

Fred A. Dente, P.E.
Principal / Office Manager

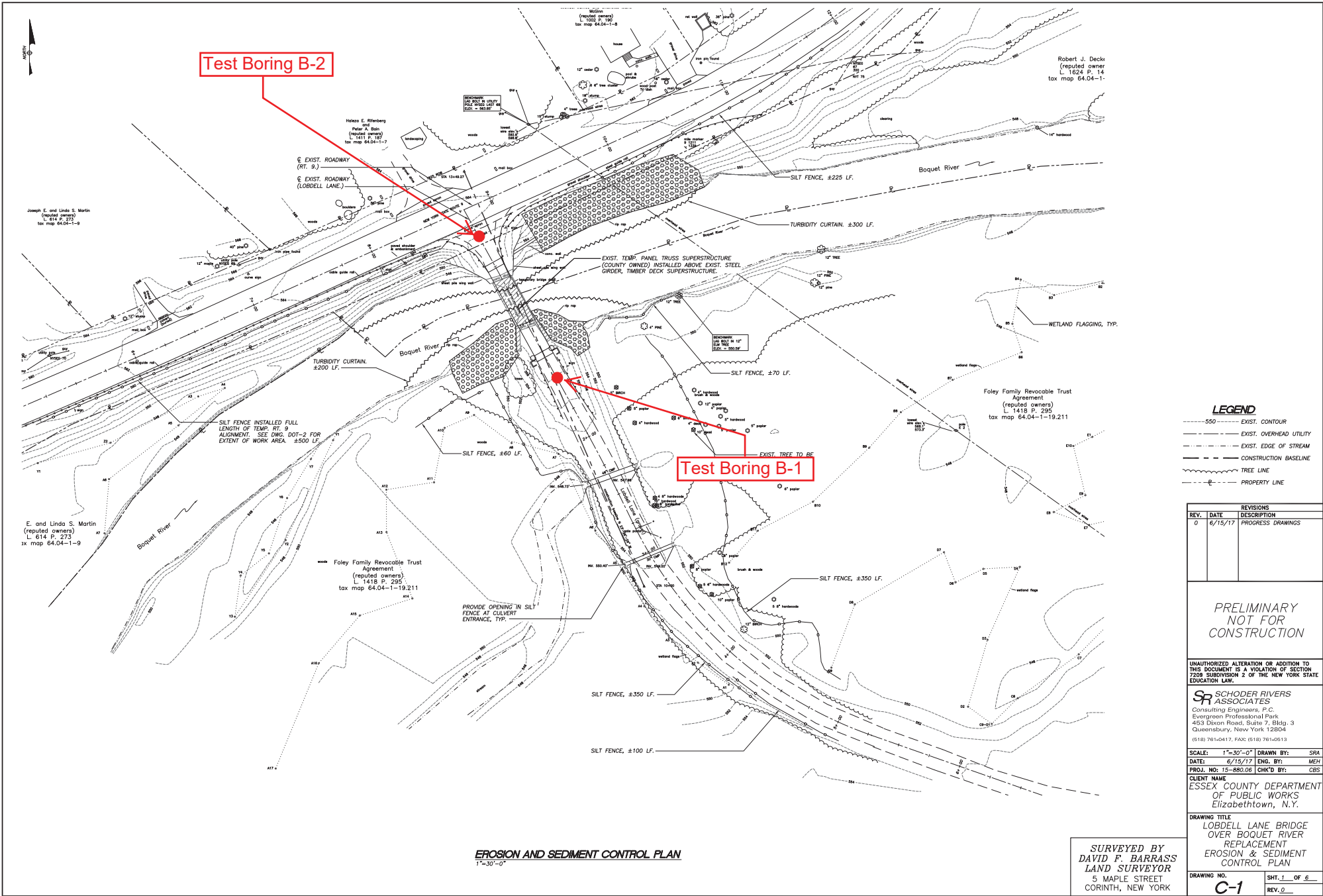
4/17/18

Attachments:

- Site Plan with Boring Locations
- Test Boring Logs and Key
- Laboratory Gradation Test Results

SUBSURFACE INVESTIGATION PLAN

**Lobdell Lane Bridge
Elizabethtown, NY**



Test Boring B-2

Test Boring B-1

LEGEND

- 550--- EXIST. CONTOUR
- EXIST. OVERHEAD UTILITY
- EXIST. EDGE OF STREAM
- CONSTRUCTION BASELINE
- TREE LINE
- PROPERTY LINE

REVISIONS	
REV.	DESCRIPTION
0	6/15/17 PROGRESS DRAWINGS

**PRELIMINARY
NOT FOR
CONSTRUCTION**

UNAUTHORIZED ALTERATION OR ADDITION TO THIS DOCUMENT IS A VIOLATION OF SECTION 7208 SUBDIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

SCHODER RIVERS ASSOCIATES
 Consulting Engineers, P.C.
 Evergreen Professional Park
 453 Dixon Road, Suite 7, Bldg. 3
 Queensbury, New York 12804
 (518) 781-0417, FAX: (518) 781-0513

SCALE: 1"=30'-0" DRAWN BY: SRA
 DATE: 6/15/17 ENG. BY: MEH
 PROJ. NO.: 15-880.06 CHK'D BY: CBS
 CLIENT NAME:
 ESSEX COUNTY DEPARTMENT
 OF PUBLIC WORKS
 Elizabethtown, N.Y.

DRAWING TITLE
 LOBDELL LANE BRIDGE
 OVER BOQUET RIVER
 REPLACEMENT
 EROSION & SEDIMENT
 CONTROL PLAN

DRAWING NO. **C-1** SH. 1 OF 6
 REV. 0

EROSION AND SEDIMENT CONTROL PLAN
 1"=30'-0"

**SURVEYED BY
DAVID F. BARRASS
LAND SURVEYOR**
 5 MAPLE STREET
 CORINTH, NEW YORK

TEST BORING LOGS AND KEY

**Lobdell Lane Bridge
Elizabethtown, NY**

INTERPRETATION OF SUBSURFACE LOGS

The Subsurface Logs present observations and the results of tests performed in the field by the Driller, Technicians, Geologists and Geotechnical Engineers as noted. Soil/Rock Classifications are made visually, unless otherwise noted, on a portion of the materials recovered through the sampling process and may not necessarily be representative of the materials between sampling intervals or locations.

The following defines some of the terms utilized in the preparation of the Subsurface Logs.

SOIL CLASSIFICATIONS

Soil Classifications are visual descriptions on the basis of the Unified Soil Classification ASTM D-2487 and USBR, 1973 with additional comments by weight of constituents by BUHRMASTER. The soil density or consistency is based on the penetration resistance determined by ASTM METHOD D1586. Soil Moisture of the recovered materials is described as DRY, MOIST, WET or SATURATED.

SIZE DESCRIPTION		RELATIVE DENSITY/CONSISTENCY (basis ASTM D1586)			
SOIL TYPE	PARTICLE SIZE	GRANULAR SOIL		COHESIVE SOIL	
		DENSITY	BLOWS/FT.	CONSISTENCY	BLOWS/FT.
BOULDER	> 12				
COBBLE	3" - 12"	LOOSE	< 10	VERY SOFT	< 3
GRAVEL-COARSE	3" - 3/4"	FIRM	11 - 30	SOFT	4 - 5
GRAVEL - FINE	3/4" - #4	COMPACT	31 - 50	MEDIUM	6 - 15
SAND - COARSE	#4 - #10	VERY COMPACT	50 +	STIFF	16 - 25
SAND - MEDIUM	#10 - #40			HARD	25 +
SAND - FINE	#40 - #200				
SILT/NONPLASTIC	< #200				
CLAY/PLASTIC	< #200				

SOIL STRUCTURE		RELATIVE PROPORTION OF SOIL TYPES	
STRUCTURE	DESCRIPTION	DESCRIPTION	% OF SAMPLE BY WEIGHT
LAYER	6" THICK OR GREATER	AND	35 - 50
SEAM	6" THICK OR LESS	SOME	20 - 35
PARTING	LESS THAN 1/4" THICK	LITTLE	10 - 20
VARVED	UNIFORM HORIZONTAL PARTINGS OR SEAMS	TRACE	LESS THAN 10

Note that the classification of soils or soil like materials is subject to the limitations imposed by the size of the sampler, the size of the sample and its degree of disturbance and moisture.

ROCK CLASSIFICATIONS

Rock Classifications are visual descriptions on the basis of the Driller's, Technician's, Geologist's or Geotechnical Engineer's observations of the coring activity and the recovered samples applying the following classifications.

CLASSIFICATION TERM	DESCRIPTION
VERY HARD	NOT SCRATCHED BY KNIFE
HARD	SCRATCHED WITH DIFFICULTY
MEDIUM HARD	SCRATCHED EASILY
SOFT	SCRATCHED WITH FINGERNAIL
VERY WEATHERED	DISINTEGRATED WITH NUMEROUS SOIL SEAM
WEATHERED	SLIGHT DISINTEGRATION, STAINING, NO SEAMS
SOUND	NO EVIDENCE OF ABOVE
MASSIVE	ROCK LAYER GREATER THAN 36" THICK
THICK BEDDED	ROCK LAYER 12" - 36"
BEDDED	ROCK LAYER 4" - 12"
THIN BEDDED	ROCK LAYER 1" - 4"
LAMINATED	ROCK LAYER LESS THAN 1"
FRACTURES	NATURAL BREAKS AT SOME ANGLE TO BEDS

Core sample recovery is expressed as percent recovered of total sampled. The ROCK QUALITY DESIGNATION (RQD) is the total length of core sample pieces exceeding 4" length divided by the total core sample length for N size cored.

GENERAL

- Soil and Rock classifications are made visually on samples recovered. The presence of Gravel, Cobbles and Boulders will influence sample recovery classification density/consistency determination.
- Groundwater, if encountered, was measured and its depth recorded at the time and under the conditions as noted.
- Topsoil or pavements, if present, were measured and recorded at the time and under the conditions as noted.
- Stratification Lines are approximate boundaries between soil types. These transitions may be gradual or distinct and are approximated.

PROJECT: Lobdell Lane over Boquet River

DATE

START: 2/08/18

FINISH: 2/08/18

LOCATION: Elizabethtown, New York

METHODS: 3-1/4" I.D. Hollow Stem Augers

CLIENT: Essex County DPW

with ASTM D1586 Sampling

JOB NUMBER: JB175555

SURFACE ELEVATION: ± 560'

DRILL TYPE: CME 45 Trailer Mounted Rig

CLASSIFICATION: O. Burns / E. Gravelle

SAMPLE		BLOWS ON SAMPLER					CLASSIFICATION / OBSERVATIONS
DEPTH	#	6"	12"	18"	24"	N	
							Data from 0' to 50' from boring on 5/4/16
5'	1	1	2				FILL: Brown/Gray Fine to Coarse SAND and GRAVEL, trace silt Grades Little Gravel, trace silt Grades Some Gravel Similar with rootlets noted Grades Little Gravel
				3	2	5	
	2	4	4				
				6	7	10	
	3	3	4				
10'	4	6	2				Grades Dark Brown (MOIST, LOOSE) Dark Brown Fine SAND and SILT (MOIST, LOOSE) Brown Mottled Fine to Medium Sand, Little Silt (WET, LOOSE) Brown/Orange GRAVEL, Some Fine to Coarse Sand, trace silt (WET, LOOSE TO FIRM) Gray Fine SAND, Some Silt
				2	3	6	
	5	2	1				
				1	2	2	
	6	2	1				
15'				1	2	2	Brown/Orange GRAVEL, Some Fine to Coarse Sand, trace silt (WET, LOOSE TO FIRM) Gray Fine SAND, Some Silt
				1	2	2	
	7	1	1				
				2	4	3	
	8	2	1/18"				
20'				-	-	1	Gray Fine SAND, Some Silt Similar
				3	18	3	
	9	1/12"	-				
				14	8	28	
	10	12	14				
25'							Similar
	11	2	4				
				3	3	7	

PROJECT: Lobdell Lane over Boquet River

DATE

START: 2/08/18

FINISH: 2/08/18

LOCATION: Elizabethtown, New York

METHODS: 3-1/4" I.D. Hollow Stem Augers

CLIENT: Essex County DPW

with ASTM D1586 Sampling

JOB NUMBER: JB175555

SURFACE ELEVATION: ± 560'

DRILL TYPE: CME 45 Trailer Mounted Rig

CLASSIFICATION: O. Burns / E. Gravelle

SAMPLE		BLOWS ON SAMPLER					CLASSIFICATION / OBSERVATIONS
DEPTH	#	6"	12"	18"	24"	N	
65'	3	WH	WH				Gray SILT, Little Clay, Little Sand
				WH	WH	WH	
65'	4	WH	WH				Gray SILT, trace to Some Clay
				WH	1	WH	
70'	5	WH	WH				Similar
				3	5	3	
75'	6	2	8				Gray CLAY, Some Silt, Little Sand
				5	2	13	
80'	7	2	6				Similar
				8	5	14	
85'	8	WH	1				Gray SILT, trace fine sand, few partings CLAY
				1	2	2	

PROJECT: Lobdell Lane over Boquet River

DATE

START: 2/08/18

FINISH: 2/08/18

LOCATION: Elizabethtown, New York

METHODS: 3-1/4" I.D. Hollow Stem Augers

CLIENT: Essex County DPW

with ASTM D1586 Sampling

JOB NUMBER: JB175555

SURFACE ELEVATION: ± 560'

DRILL TYPE: CME 45 Trailer Mounted Rig

CLASSIFICATION: O. Burns / E. Gravelle

SAMPLE		BLOWS ON SAMPLER					CLASSIFICATION / OBSERVATIONS
DEPTH	#	6"	12"	18"	24"	N	
95'	9	1	1				Gray SAND and SILT, Some Clay, trace fine gravel
				6	9	7	
100'	10	3	8				Gray SILT, trace to Little Clay with thin seams Fine to Medium SAND, Some Silt
				4	6	12	
105'	11	3	6				Gray SILT, Little Fine to Medium Sand (SATURATED, LOOSE TO FIRM/V. SOFT TO MEDIUM) Boring Ended at 102.0'
				5	4	11	
110'							No measurable groundwater in augers at completion of drilling and sampling.
115'							

PROJECT: Lobdell Lane over Boquet River

DATE

START: 2/13/18

FINISH: 2/13/18

LOCATION: Elizabethtown, New York

METHODS: 3-1/4" I.D. Hollow Stem Augers

CLIENT: Essex County DPW

with ASTM D1586 Sampling

JOB NUMBER: JB175555

SURFACE ELEVATION: ± 564'

DRILL TYPE: CME 45 Trailer Mounted Rig

CLASSIFICATION: O. Burns / E. Gravelle

SAMPLE		BLOWS ON SAMPLER					CLASSIFICATION / OBSERVATIONS
DEPTH	#	6"	12"	18"	24"	N	
	11	1	2				Data from 0' to 50' from boring on 5/4/16
				1	2	3	Gray SILT and Fine SAND
35'	12	1	1				Similar
				2	4	3	
40'	13	1	2				Similar
				3	3	5	
45'	14	7	9				(SATURATED, FIRM TO LOOSE)
				10	11	19	Brown/Gray SILT with occasional partings Fine to Medium SAND or CLAY
50'	1	5	5				Data from 50' to 102' from boring on 2/13/18
				8	13	13	Gray SILT and Fine SAND with partings SILT and/or CLAY
55'	2	7	10				Gray SILT
				12	13	22	

PROJECT: Lobdell Lane over Boquet River

DATE

START: 2/13/18

FINISH: 2/13/18

LOCATION: Elizabethtown, New York

METHODS: 3-1/4" I.D. Hollow Stem Augers

CLIENT: Essex County DPW

with ASTM D1586 Sampling

JOB NUMBER: JB175555

SURFACE ELEVATION: ± 564'

DRILL TYPE: CME 45 Trailer Mounted Rig

CLASSIFICATION: O. Burns / E. Gravelle

SAMPLE		BLOWS ON SAMPLER					CLASSIFICATION / OBSERVATIONS
DEPTH	#	6"	12"	18"	24"	N	
65'	3	13	8				Gray SILT, Some Clay, Some Sand
				8	9	16	
70'	4	WH	WH				Gray SILT with partings CLAY
				2	2	2	
75'	5	WH	2				Similar
				4	5	6	
80'	6	3	5				Gray SILT, Some Sand, Little Clay
				4	6	9	
85'	7	4	5				Similar
				7	7	12	
85'	8	4	3				Similar
				9	8	12	

PROJECT: Lobdell Lane over Boquet River

DATE

START: 2/13/18

FINISH: 2/13/18

LOCATION: Elizabethtown, New York

METHODS: 3-1/4" I.D. Hollow Stem Augers

CLIENT: Essex County DPW

with ASTM D1586 Sampling

JOB NUMBER: JB175555

SURFACE ELEVATION: ± 564'

DRILL TYPE: CME 45 Trailer Mounted Rig

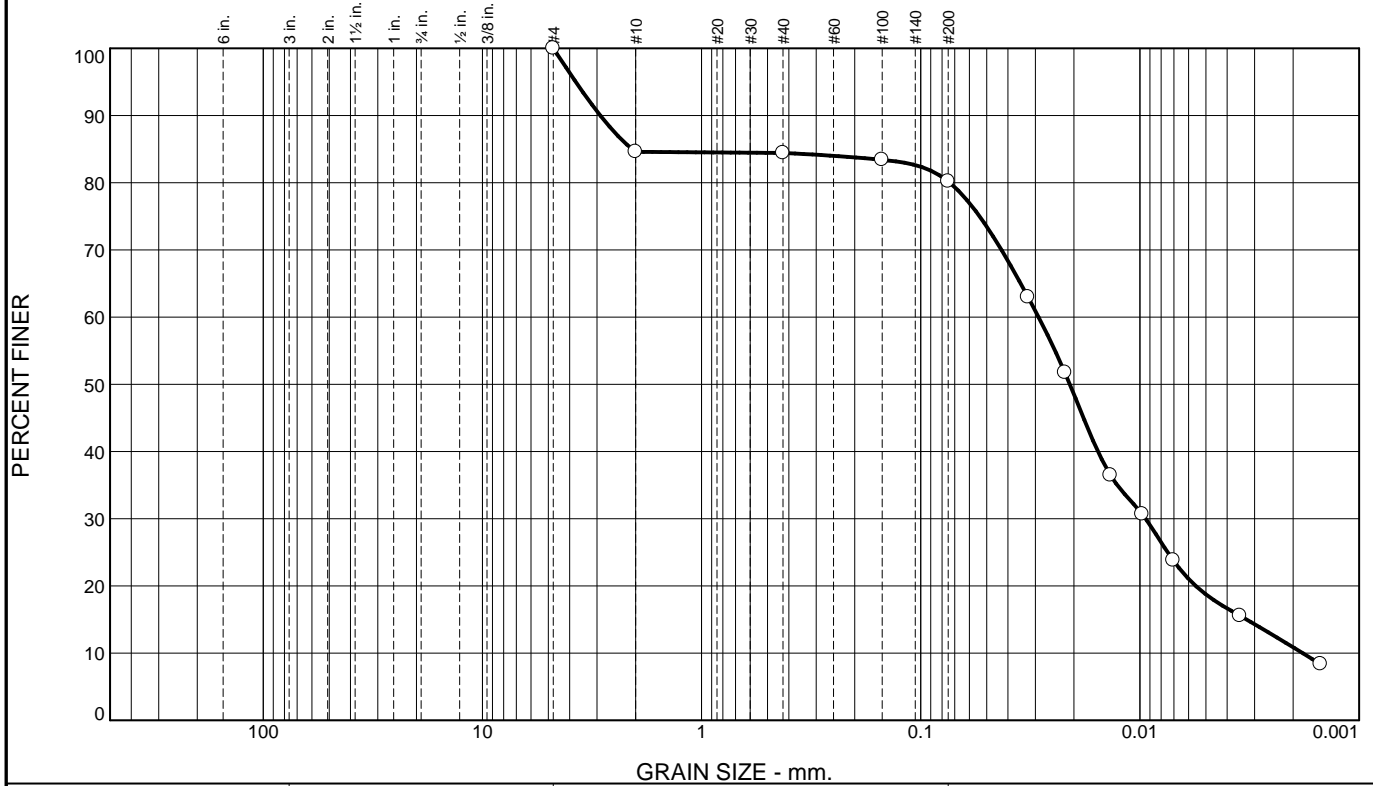
CLASSIFICATION: O. Burns / E. Gravelle

SAMPLE		BLOWS ON SAMPLER					CLASSIFICATION / OBSERVATIONS
DEPTH	#	6"	12"	18"	24"	N	
95'	9	3	6				Gray SILT and SAND, Little Clay
				7	8	13	
100'	10	4	5				Gray SILT, trace to Some Clay
				8	9	13	
105'	11	4	6				Grades trace to Little Clay, trace fine sand (SATURATED, LOOSE TO FIRM / MEDIUM)
				6	11	12	
110'							Boring Ended at 102.0'
115'							No measurable groundwater in augers at completion of drilling and sampling.

LABORATORY TEST RESULTS

**Lobdell Lane Bridge
Elizabethtown, NY**

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	15.4	0.2	4.2	61.5	18.7

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	84.6		
#40	84.4		
#100	83.4		
#200	80.2		

Material Description

SILT, Little C-F-M Sand and Clay

Atterberg Limits

PL= NP LL= NP PI= NP

Coefficients

D₉₀= 2.8975 D₈₅= 2.0755 D₆₀= 0.0290
D₅₀= 0.0209 D₃₀= 0.0094 D₁₅= 0.0033
D₁₀= 0.0018 C_u= 16.02 C_c= 1.69

Classification

USCS= ML AASHTO= A-4(0)

Remarks

Per ASTM D422 Washed

* (no specification provided)

Source of Sample: Soil Borings Depth: 60'-62' Date: 3-1-18
Sample Number: 516 B-1/S-3

EVERGREEN TESTING, INC. A Terracon Company Watervliet, NY	Client: Essex Co. DPW Project: Lobdell Lane Bridge Elizabethtown, NY Project No: JB175555
Figure 516	

Tested By: AB Checked By: FD

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	17.4	0.2	2.8	28.0	51.6

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	82.6		
#40	82.4		
#100	81.2		
#200	79.6		

Material Description

CLAY, Some Silt and C-F-M Sand

Atterberg Limits

PL= NP LL= NP PI= NP

Coefficients

D₉₀= 3.0861 D₈₅= 2.3711 D₆₀= 0.0077
D₅₀= 0.0046 D₃₀= 0.0019 D₁₅=
D₁₀= C_u= C_c=

Classification

USCS= ML AASHTO= A-4(0)

Remarks

Per ASTM D422 Washed

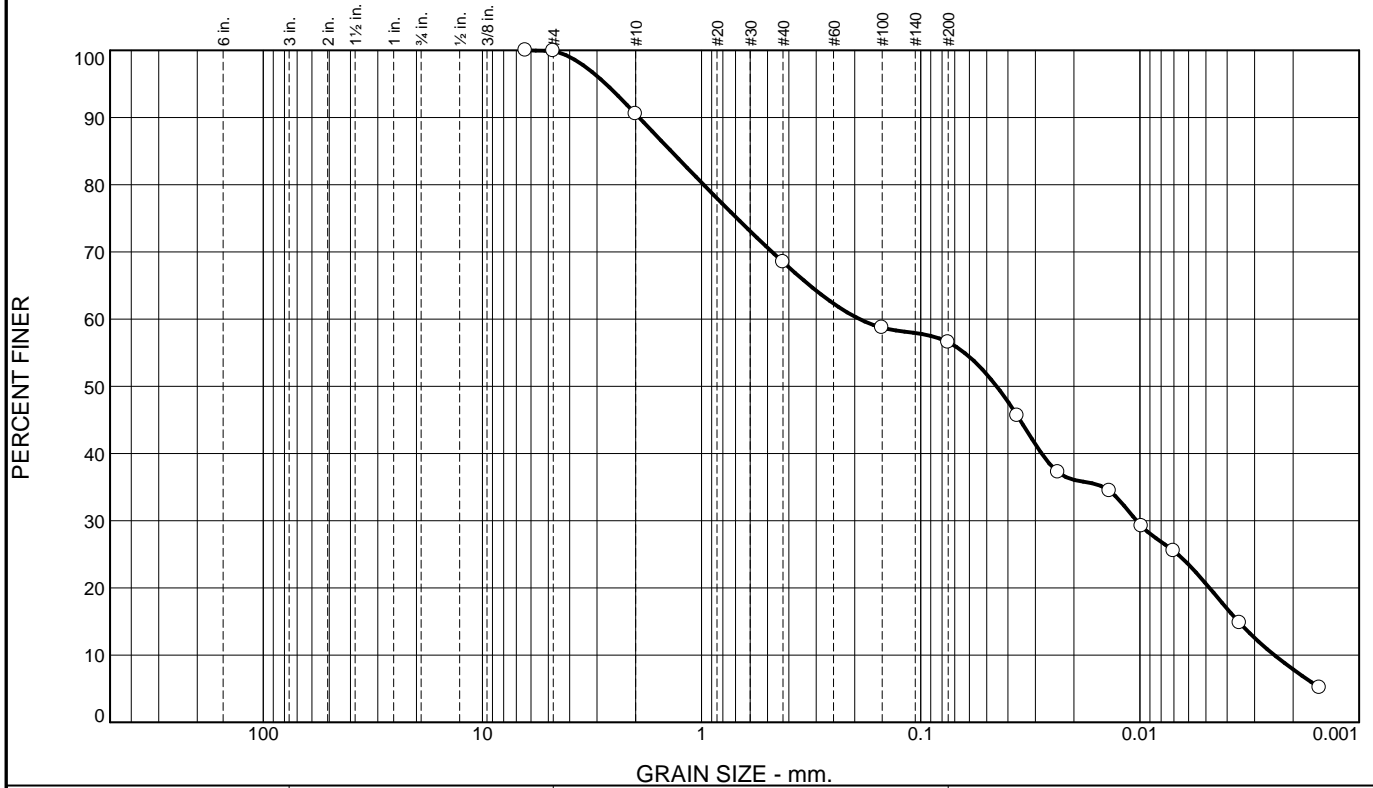
* (no specification provided)

Source of Sample: Soil Borings Depth: 75'-77' Date: 3-1-18
Sample Number: 517 B-1/S-6

EVERGREEN TESTING, INC. A Terracon Company Watervliet, NY	Client: Essex Co. DPW Project: Lobdell Lane Bridge Elizabethtown, NY Project No: JB175555
Figure 517	

Tested By: AB Checked By: FD

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.1	9.4	22.0	11.9	36.0	20.6

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
0.25"	100.0		
#4	99.9		
#10	90.5		
#40	68.5		
#100	58.7		
#200	56.6		

Material Description

M-F-C SAND and SILT, Some Clay, trace fine gravel

Atterberg Limits
 PL= NP LL= NP PI= NP

Coefficients

D ₉₀ = 1.9301	D ₈₅ = 1.3771	D ₆₀ = 0.1901
D ₅₀ = 0.0451	D ₃₀ = 0.0104	D ₁₅ = 0.0036
D ₁₀ = 0.0024	C _u = 78.04	C _c = 0.23

Classification
 USCS= ML AASHTO= A-4(0)

Remarks
 Per ASTM D422 Washed

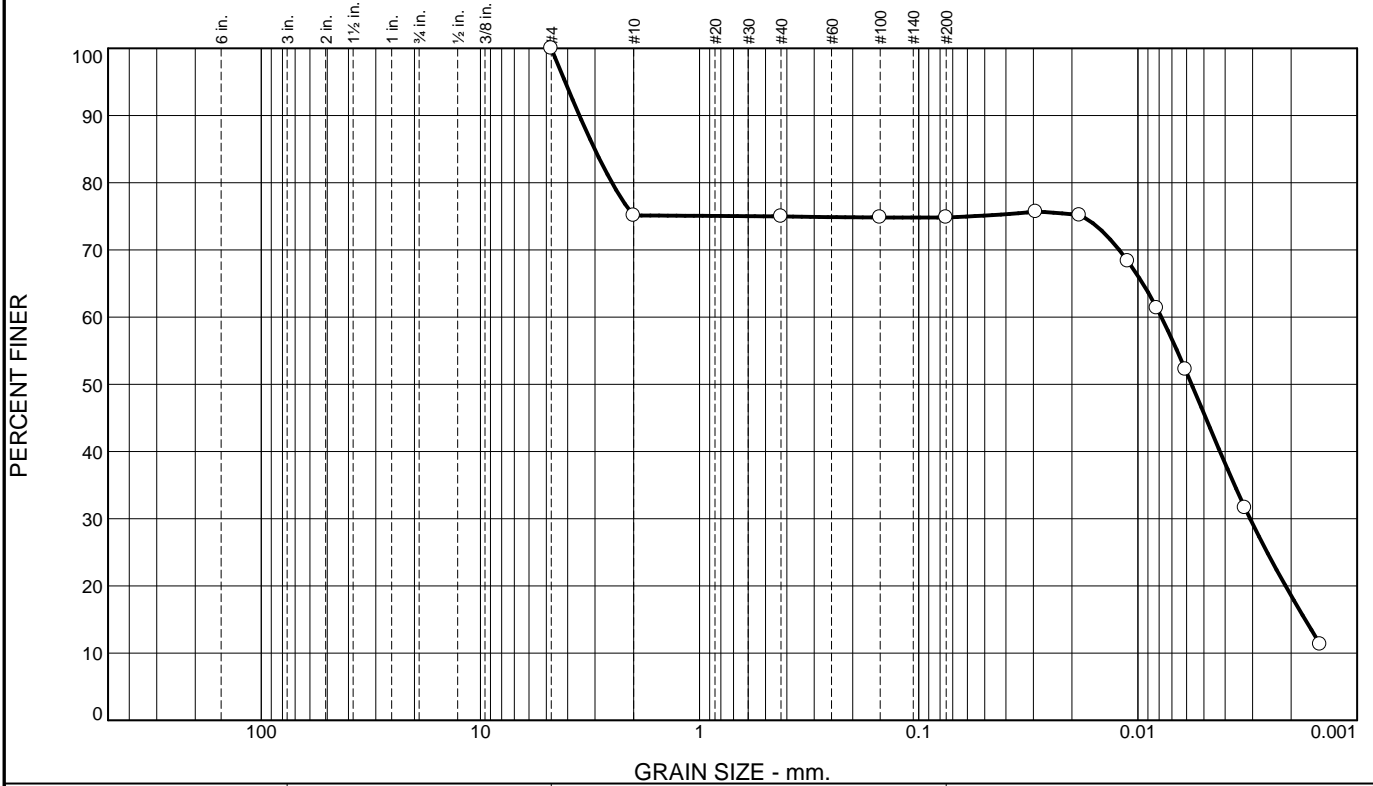
* (no specification provided)

Source of Sample: Soil Borings Depth: 90'-92' Date: 3-1-18
 Sample Number: 518 B-1/S-9

EVERGREEN TESTING, INC. A Terracon Company Watervliet, NY	Client: Essex Co. DPW Project: Lobdell Lane Bridge Elizabethtown, NY Project No: JB175555
Figure 518	

Tested By: AB Checked By: FD

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	24.9	0.1	0.2	29.1	45.7

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	75.1		
#40	75.0		
#100	74.8		
#200	74.8		

Material Description

CLAY, Some Silt and C-F-M Sand

Atterberg Limits
 PL= NP LL= NP PI= NP

Coefficients
 D₉₀= 3.5340 D₈₅= 3.0105 D₆₀= 0.0078
 D₅₀= 0.0057 D₃₀= 0.0031 D₁₅= 0.0017
 D₁₀= C_u= C_c=

Classification
 USCS= ML AASHTO= A-4(0)

Remarks
 Per ASTM D422 Washed

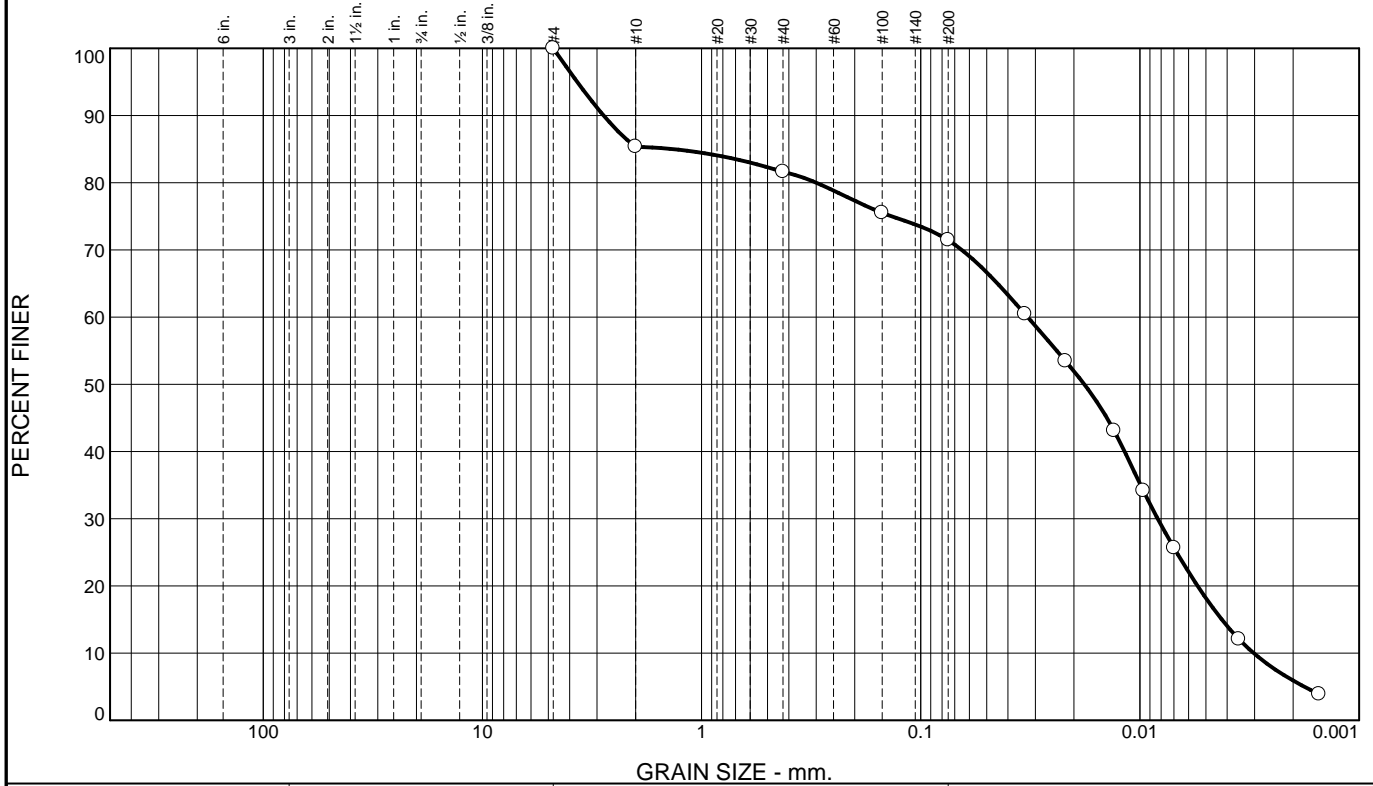
* (no specification provided)

Source of Sample: Soil Borings Depth: 60'-62' Date: 3-1-18
 Sample Number: 519 B-2/S-3

EVERGREEN TESTING, INC. A Terracon Company Watervliet, NY	Client: Essex Co. DPW Project: Lobdell Lane Bridge Elizabethtown, NY Project No: JB175555
Figure 519	

Tested By: AB Checked By: FD

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	14.7	3.7	10.2	53.2	18.2

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	85.3		
#40	81.6		
#100	75.5		
#200	71.4		

Material Description

SILT, Some C-F-M Sand, Little Clay

Atterberg Limits
 PL= NP LL= NP PI= NP

Coefficients

D ₉₀ = 2.8013	D ₈₅ = 1.3571	D ₆₀ = 0.0325
D ₅₀ = 0.0179	D ₃₀ = 0.0083	D ₁₅ = 0.0042
D ₁₀ = 0.0030	C _u = 10.75	C _c = 0.70

Classification
 USCS= ML AASHTO= A-4(0)

Remarks
 Per ASTM D422 Washed

* (no specification provided)

Source of Sample: Soil Borings Depth: 75'-77' Date: 3-1-18
 Sample Number: 520 B-2/S-6

EVERGREEN TESTING, INC. A Terracon Company Watervliet, NY	Client: Essex Co. DPW Project: Lobdell Lane Bridge Elizabethtown, NY Project No: JB175555	Figure 520
--	--	------------

Tested By: AB Checked By: FD

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	8.2	9.6	25.7	44.2	12.3

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	91.8		
#40	82.2		
#100	68.7		
#200	56.5		

Material Description

SILT and F-M-C SAND, Little Clay

Atterberg Limits

PL= NP LL= NP PI= NP

Coefficients

D ₉₀ = 1.5012	D ₈₅ = 0.6008	D ₆₀ = 0.0875
D ₅₀ = 0.0594	D ₃₀ = 0.0161	D ₁₅ = 0.0061
D ₁₀ = 0.0039	C _u = 22.15	C _c = 0.75

Classification

USCS= ML AASHTO= A-4(0)

Remarks

Per ASTM D422 Washed

* (no specification provided)

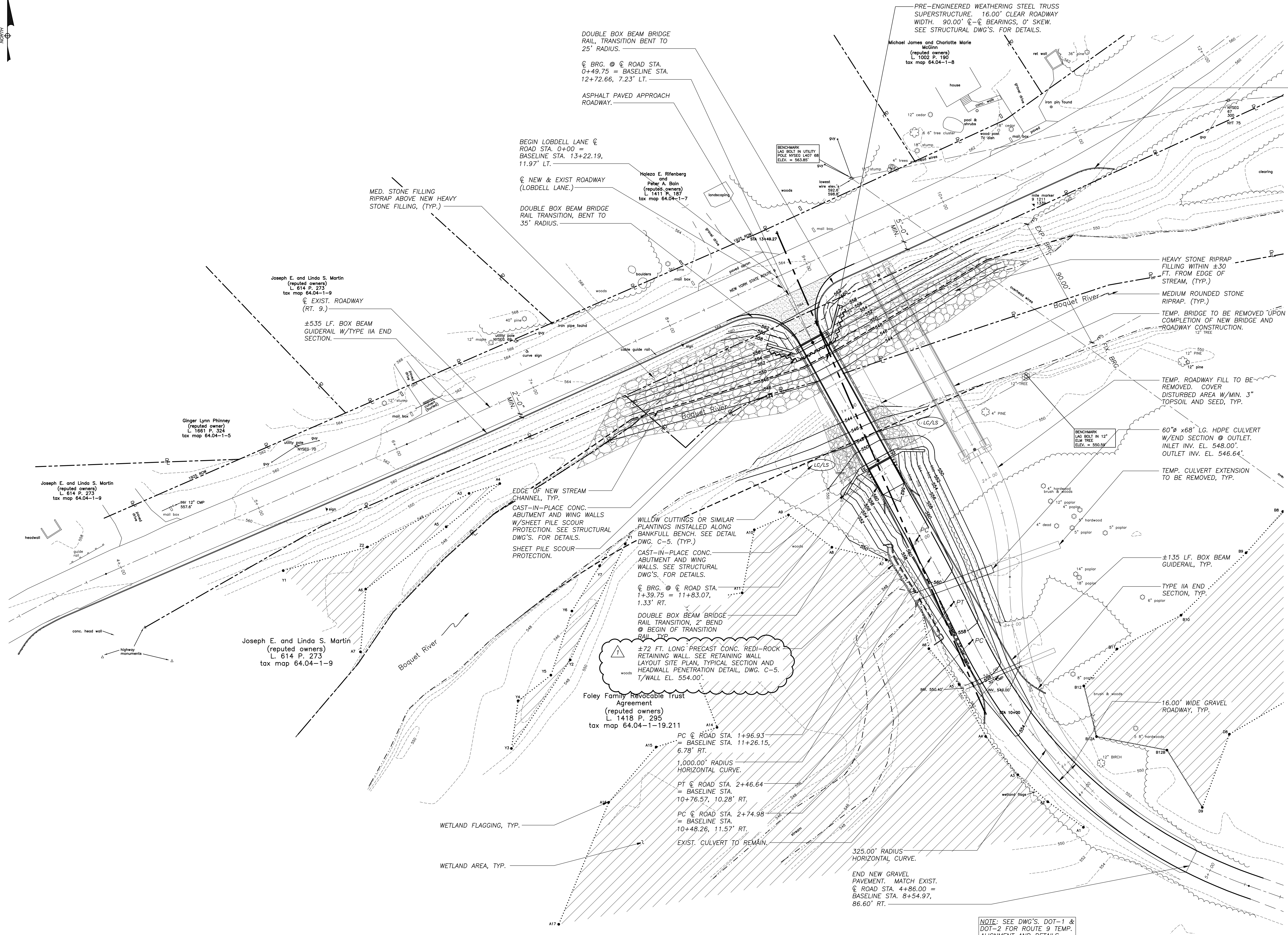
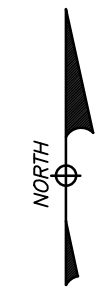
Source of Sample: Soil Borings Depth: 90'-92'
 Sample Number: 521 B-2/S-9

Date: 3-1-18

EVERGREEN TESTING, INC. A Terracon Company Watervliet, NY	Client: Essex Co. DPW Project: Lobdell Lane Bridge Elizabethtown, NY Project No: JB175555
Figure 521	

Tested By: AB Checked By: FD

Drawings



DOUBLE BOX BEAM BRIDGE
RAIL, TRANSITION BENT TO
25' RADIUS.
C. BRG. @ C. ROAD STA.
0+49.75 = BASELINE STA.
12+72.66, 7.23' LT.
ASPHALT PAVED APPROACH
ROADWAY.

BEGIN LOBDELL LANE @
ROAD STA. 0+00 =
BASELINE STA. 13+22.19,
11.97' LT.

C. NEW & EXIST ROADWAY
(LOBDELL LANE.)

DOUBLE BOX BEAM BRIDGE
RAIL TRANSITION, BENT TO
35' RADIUS.

Joseph E. and Linda S. Martin
(reputed owners)
L. 614 P. 273
tax map 64.04-1-9
C. EXIST. ROADWAY
(RT. 9.)

±535 LF. BOX BEAM
GUIDERAIL W/TYPE IIA END
SECTION.

Ginger Lynn Phinney
(reputed owner)
L. 1691 P. 324
tax map 64.04-1-5

Joseph E. and Linda S. Martin
(reputed owners)
L. 614 P. 273
tax map 64.04-1-9

Joseph E. and Linda S. Martin
(reputed owners)
L. 614 P. 273
tax map 64.04-1-9

Foley Family Revocable Trust
(reputed owners)
L. 1418 P. 295
tax map 64.04-1-19.211

PC @ ROAD STA. 1+96.93
= BASELINE STA. 11+26.15,
6.78' RT.
1,000.00' RADIUS
HORIZONTAL CURVE.
PT @ ROAD STA. 2+46.64
= BASELINE STA.
10+76.57, 10.28' RT.
PC @ ROAD STA. 2+74.98
= BASELINE STA.
10+48.26, 11.57' RT.
EXIST. CULVERT TO REMAIN.

325.00' RADIUS
HORIZONTAL CURVE.
END NEW GRAVEL
PAVEMENT. MATCH EXIST.
C. ROAD STA. 4+86.00 =
BASELINE STA. 8+54.97,
86.60' RT.

PRE-ENGINEERED WEATHERING STEEL TRUSS
SUPERSTRUCTURE. 16.00' CLEAR ROADWAY
WIDTH. 90.00' C-C BEARINGS, 0' SKEW.
SEE STRUCTURAL DWG'S. FOR DETAILS.

Michael James and Charlotte Marie
McGinn
(reputed owners)
L. 1002 P. 190
tax map 64.04-1-8

BENCHMARK
LAG BOLT IN UTILITY
PALE W/502, 6407 86
ELEV. = 553.52'

HEAVY STONE RIPRAP
FILLING WITHIN ±30
FT. FROM EDGE OF
STREAM, (TYP.)

MEDIUM ROUNDED STONE
RIPRAP, (TYP.)

TEMP. BRIDGE TO BE REMOVED UPON
COMPLETION OF NEW BRIDGE AND
ROADWAY CONSTRUCTION.

TEMP. ROADWAY FILL TO BE
REMOVED. COVER
DISTURBED AREA W/MIN. 3"
TOPSOIL AND SEED, TYP.

60" x 68" LG. HDPE CULVERT
W/END SECTION @ OUTLET.
INLET INV. EL. 548.00'.
OUTLET INV. EL. 546.64'.

TEMP. CULVERT EXTENSION
TO BE REMOVED, TYP.

BENCHMARK
LAG BOLT IN 12"
DIA. TREE
ELEV. = 550.52'

±135 LF. BOX BEAM
GUIDERAIL, TYP.

TYPE IIA END
SECTION, TYP.

16.00' WIDE GRAVEL
ROADWAY, TYP.

±175 LF. BOX BEAM
GUIDERAIL W/TYPE IIA END
SECTION.

LEGEND

---	PROPERTY LINE
---	EXIST. CONTOUR
---	NEW CONTOUR
---	EXIST. OVERHEAD UTILITY
---	EXIST. EDGE OF STREAM
---	CONSTRUCTION BASELINE
---	TREE LINE
---	WETLAND
---	ANGULAR RIPRAP
---	ROUNDED RIPRAP

REVISIONS

REV.	DATE	DESCRIPTION
0	7/16/19	BID & CONSTRUCTION
1	8/12/19	ADDENDUM No. 1



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7209 SUBDIVISION 2 OF THE NEW YORK STATE
EDUCATION LAW.

SCHODER RIVERS ASSOCIATES
Consulting Engineers, P.C.
Evergreen Professional Park
453 Dixon Road, Suite 7, Bldg. 3
Queensbury, New York 12804
(518) 761-0417, FAX: (518) 761-0513

SCALE: 1"=30'-0" DRAWN BY: SRA
DATE: 7/16/19 ENG. BY: MEH
PROJ. NO: 15-880.06 CHK'D BY: ES/CBS

CLIENT NAME
**ESSEX COUNTY DEPARTMENT
OF PUBLIC WORKS
Elizabethtown, N.Y.**

DRAWING TITLE
**LOBDELL LANE BRIDGE
OVER BOQUET RIVER
REPLACEMENT**

SITE PLAN
DRAWING NO. **C-3** SHT. 3 OF 6
REV. 1

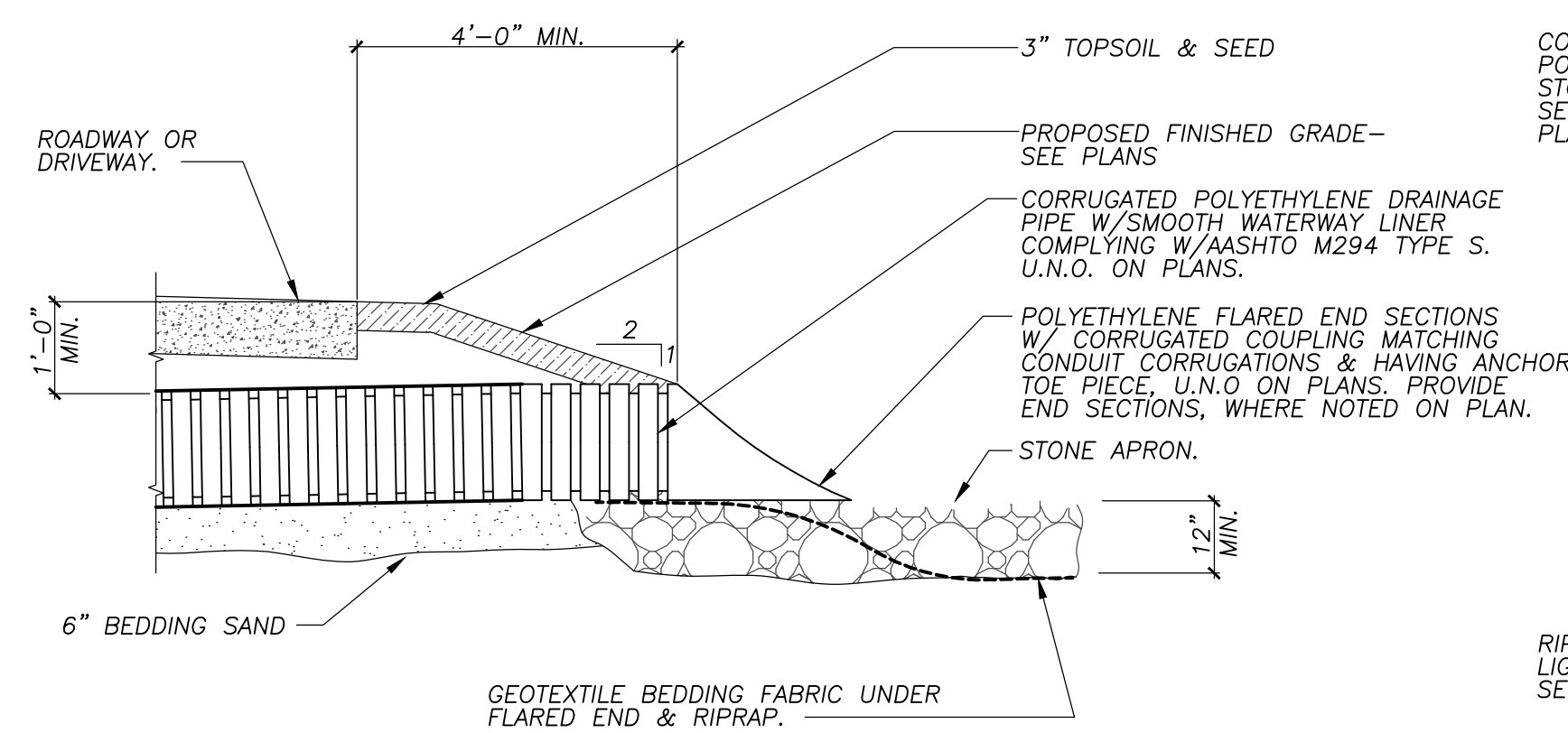
SITE PLAN
1"=30'-0"

NOTE: SEE DWG'S. DOT-1 &
DOT-2 FOR ROUTE 9 TEMP.
ALIGNMENT AND DETAILS.

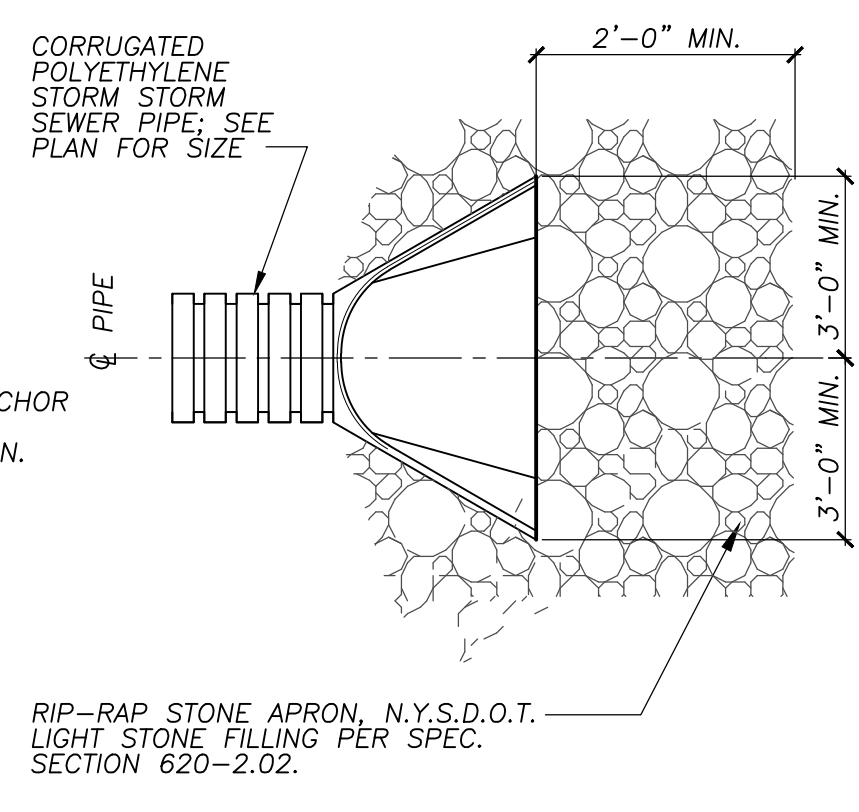
NOTE: ALL AREAS DISTURBED DURING
CONSTRUCTION NOT COVERED WITH
SITE IMPROVEMENTS OR LANDSCAPING
SHALL BE COVERED WITH MIN. 3" OF
TOPSOIL AND SEED TO ESTABLISH
DENSE GROWTH OF TURF.

NOTE: SEE DWG. DOT-2
FOR BASELINE STATION
LOCATIONS AND TIES.

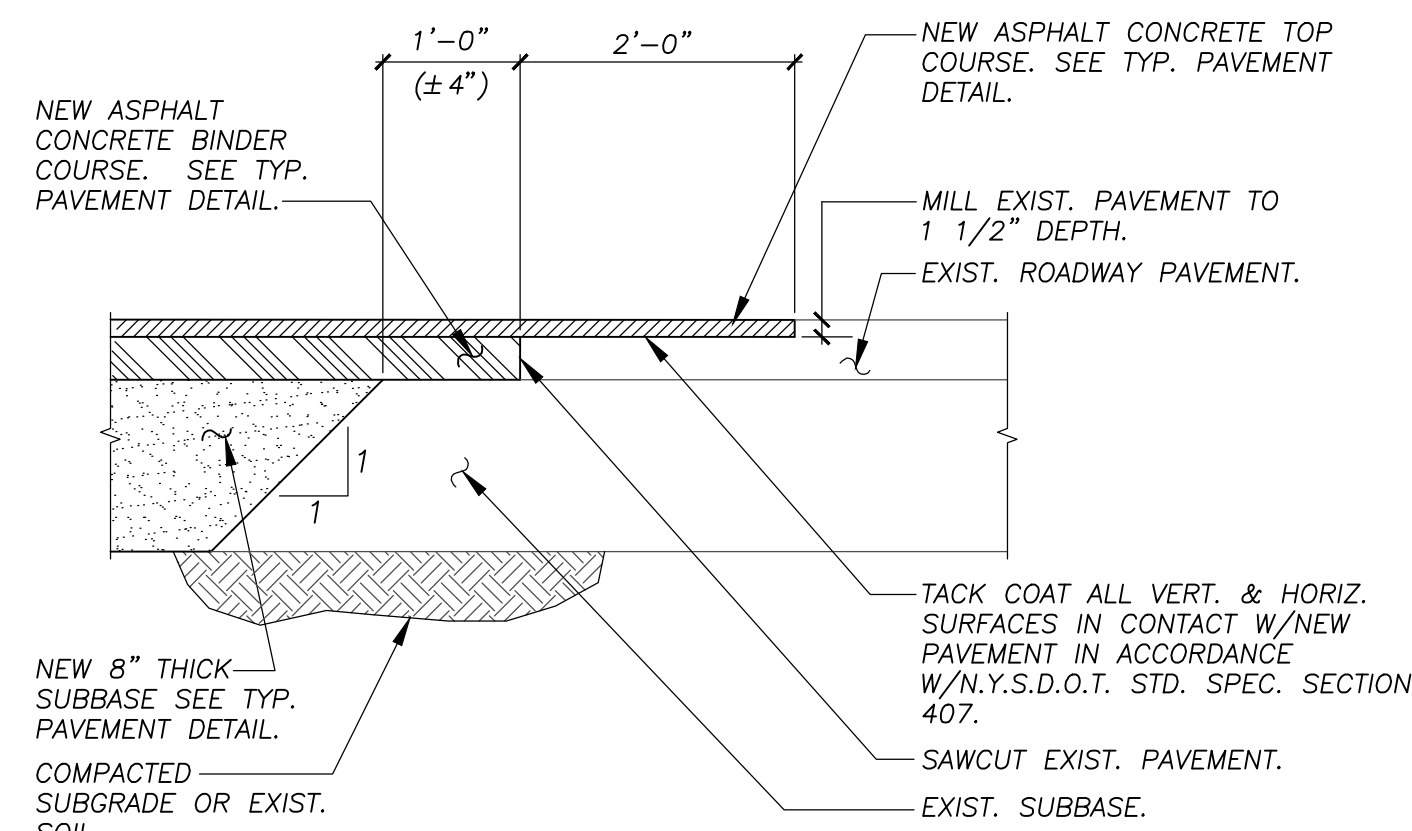
**SURVEYED BY
DAVID F. BARRASS
LAND SURVEYOR
5 MAPLE STREET
CORINTH, NEW YORK**



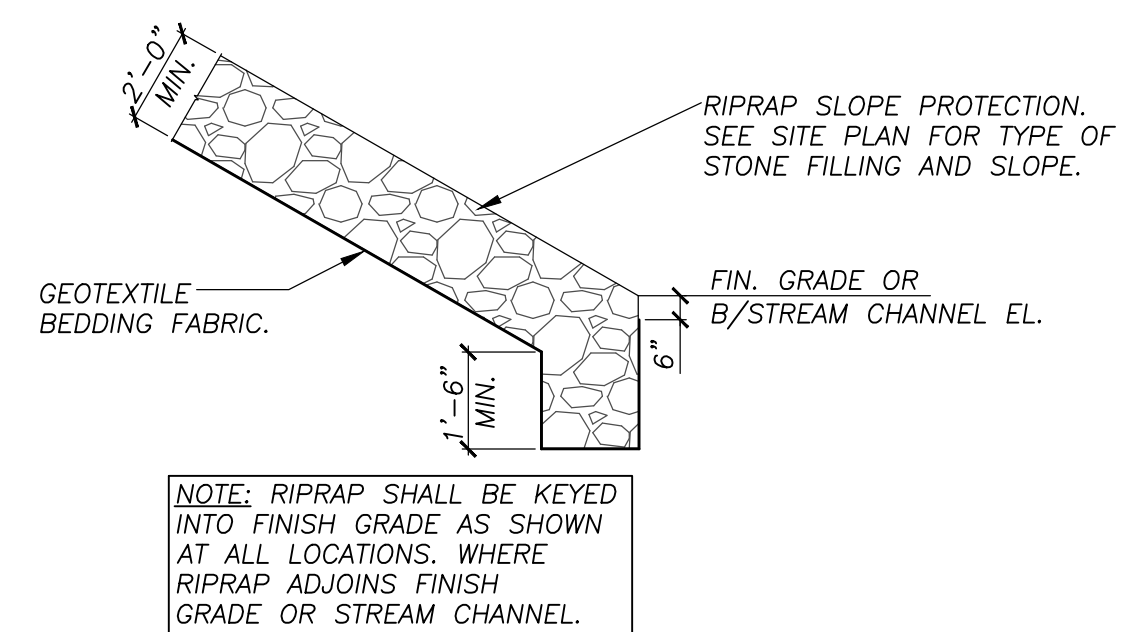
TYPICAL CULVERT DETAIL
N.T.S.



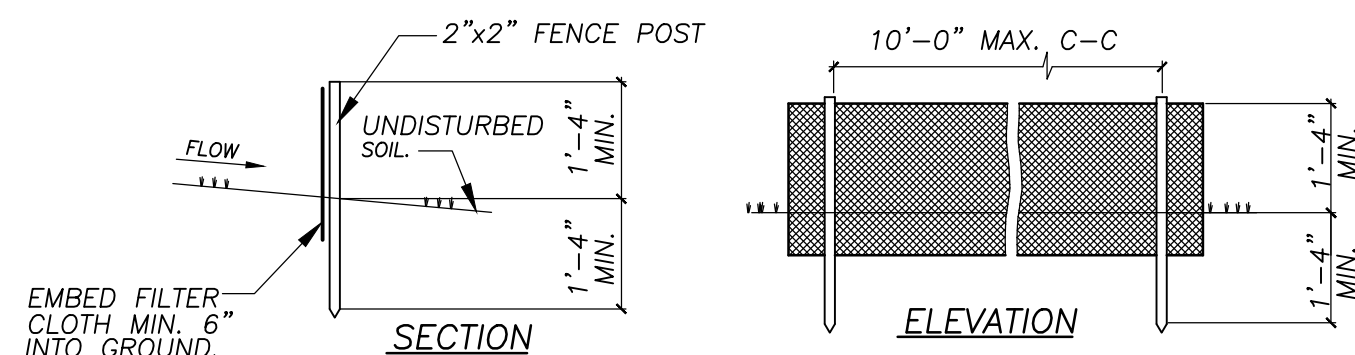
PLAN



ASPHALT PAVEMENT TRANSITION DETAIL
N.T.S.

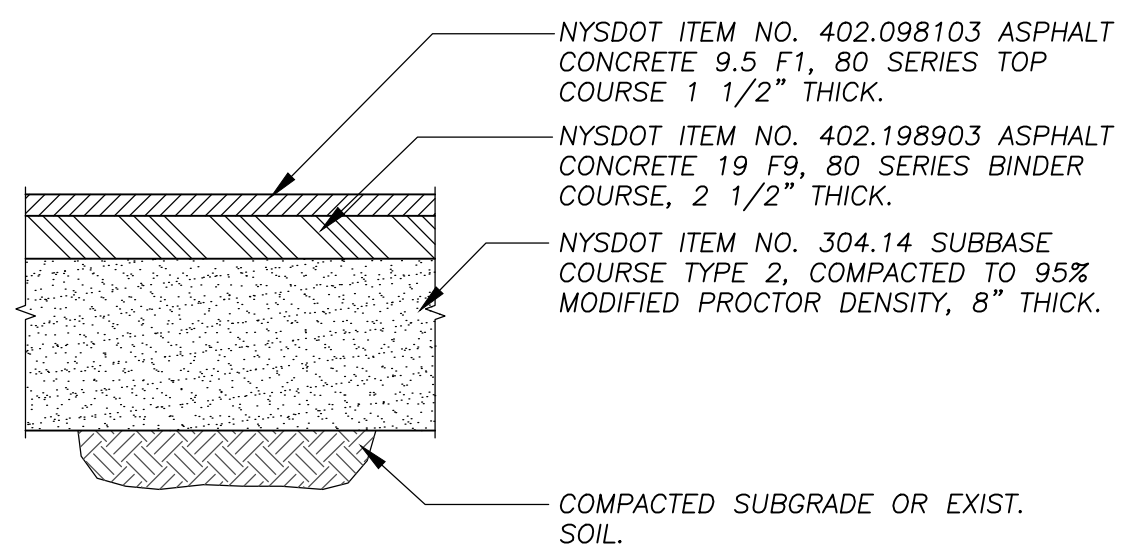


RIPRAP KEYING DETAIL
N.T.S.

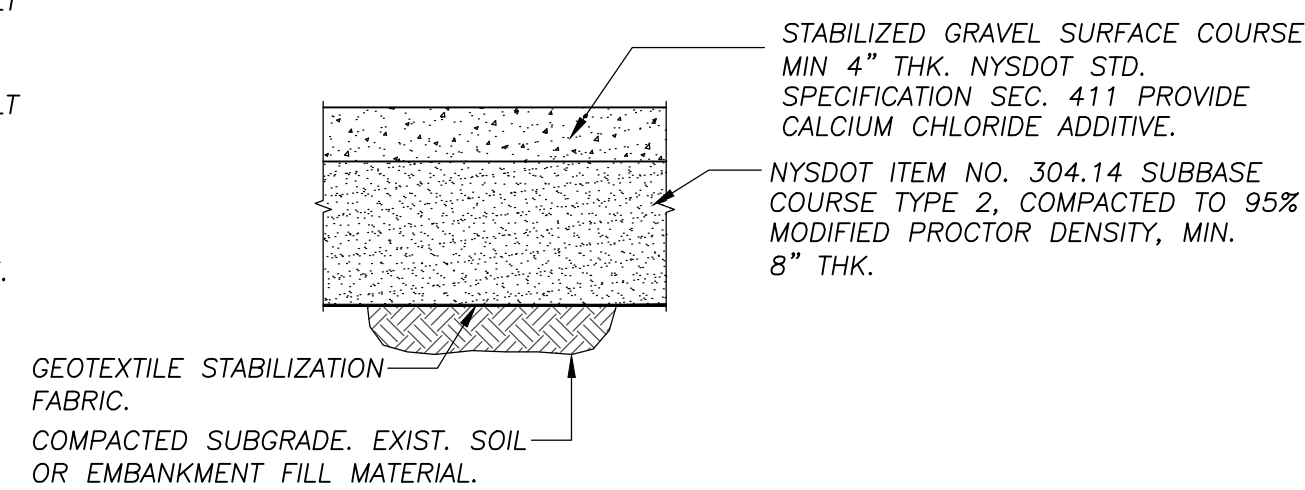


- NOTES**
1. FILTER CLOTH TO BE FASTENED SECURELY TO POSTS WITH STAPLES OR TIES AT 6" MAX. SPACING.
 2. WHEN TWO SECTIONS OF FILTER CLOTH ADJOIN EACH OTHER THEY SHALL BE OVERLAPPED BY 6" AND FOLDED.
 3. MAINTENANCE SHALL BE PERFORMED AS NEEDED AND MATERIAL REMOVED WHEN "BULGES" DEVELOP IN THE SILT FENCE.

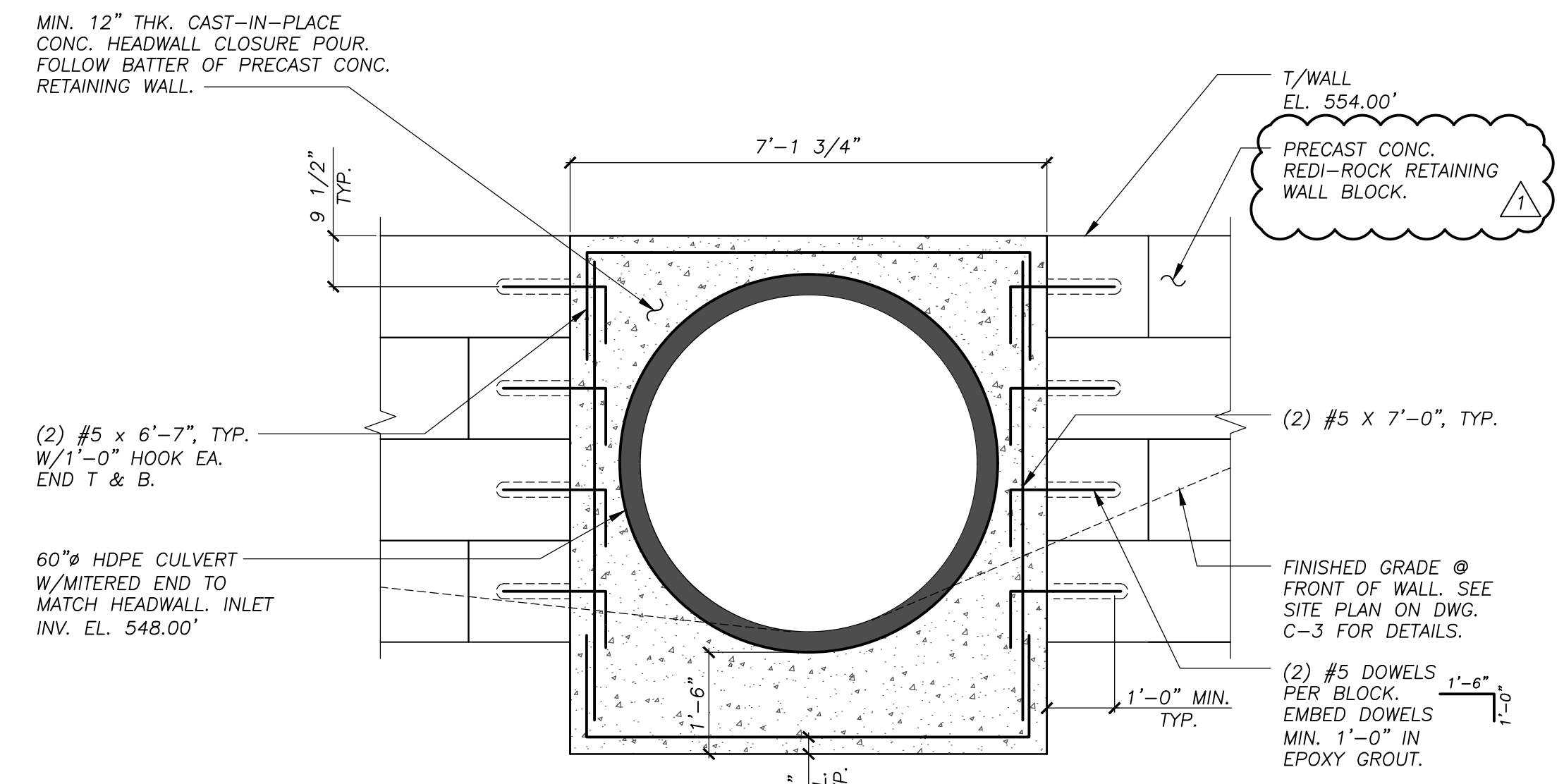
SILT FENCE DETAIL
N.T.S.



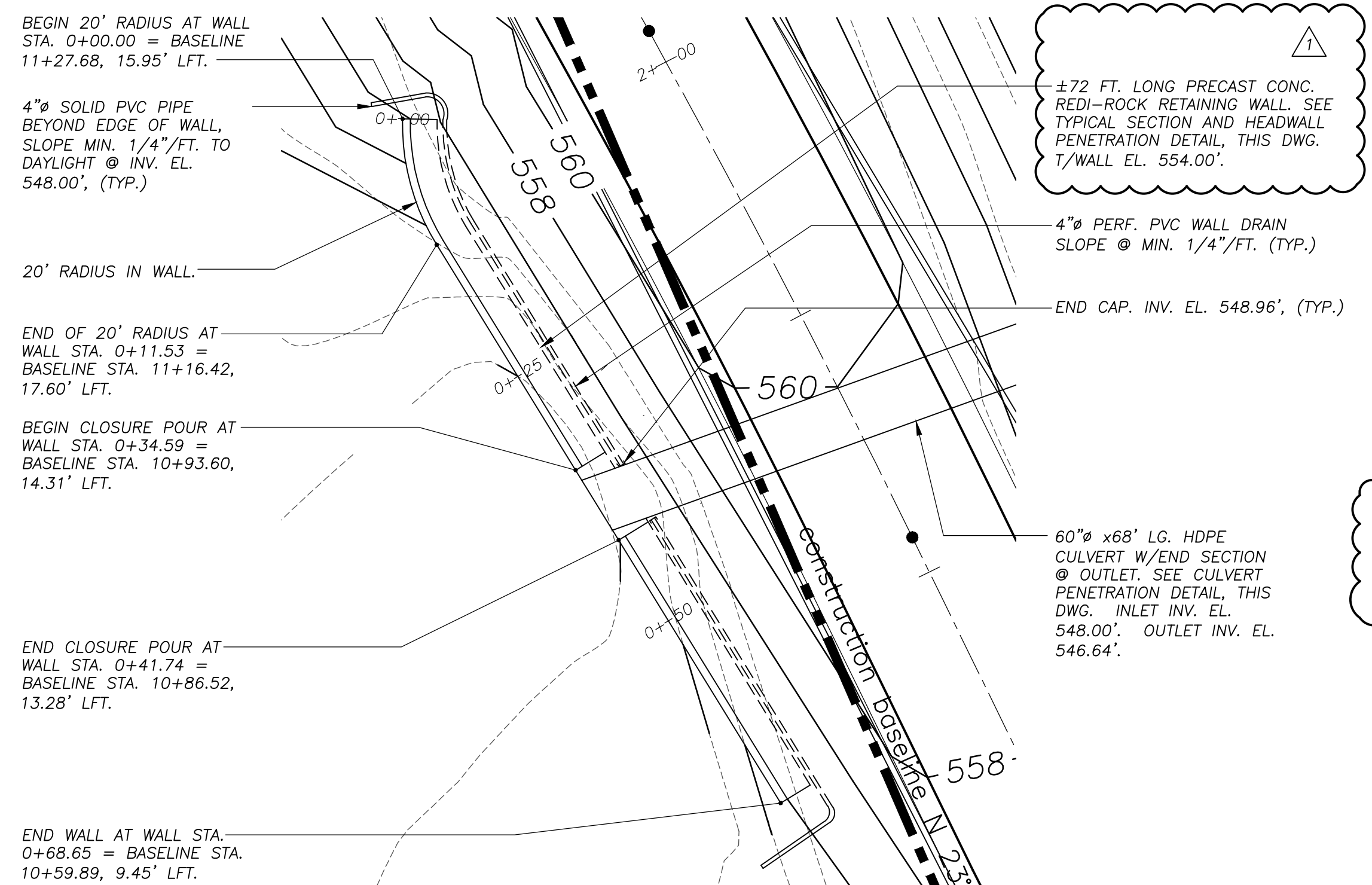
TYPICAL ASPHALT PAVEMENT DETAIL
N.T.S.



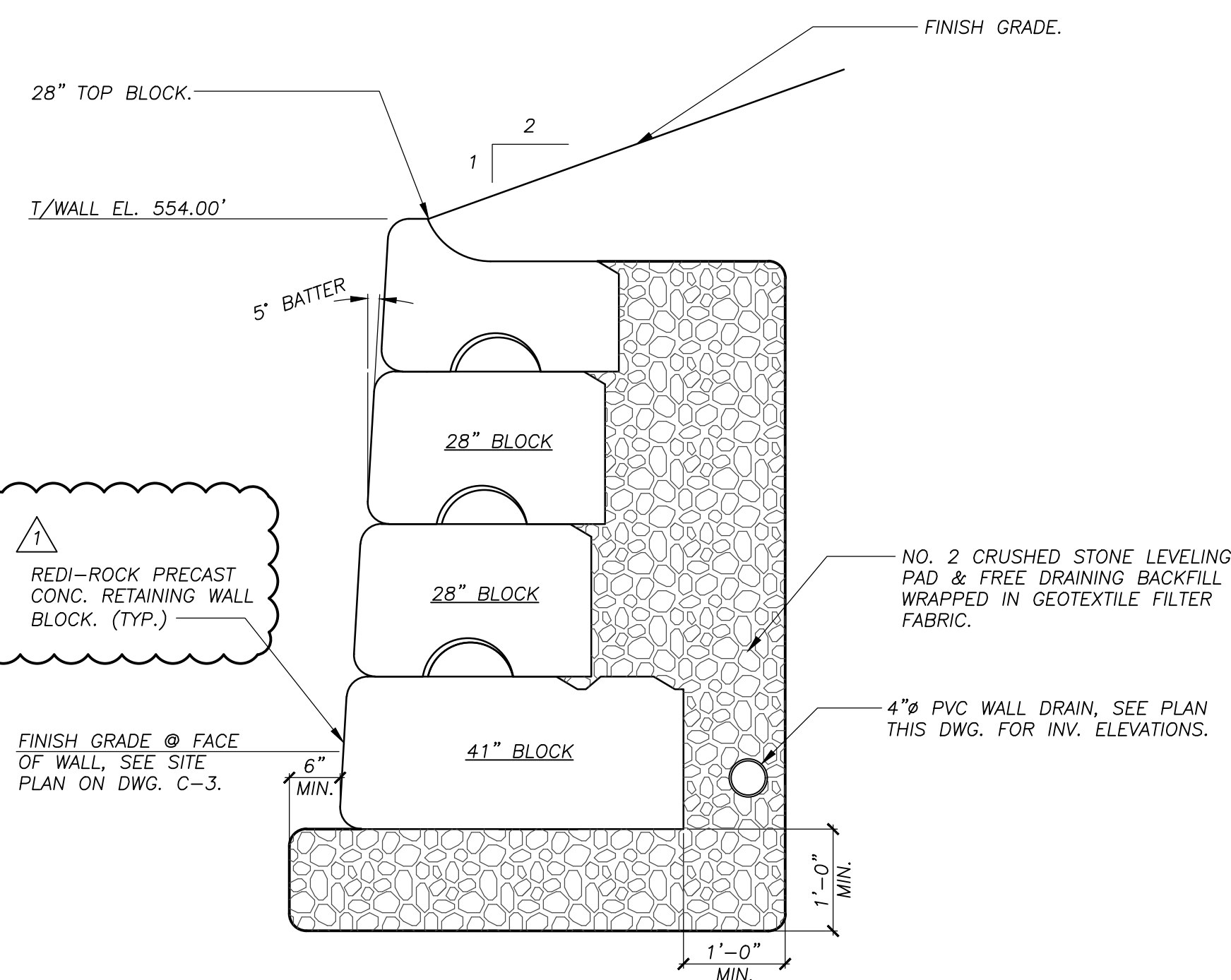
TYPICAL GRAVEL PAVEMENT DETAIL
N.T.S.



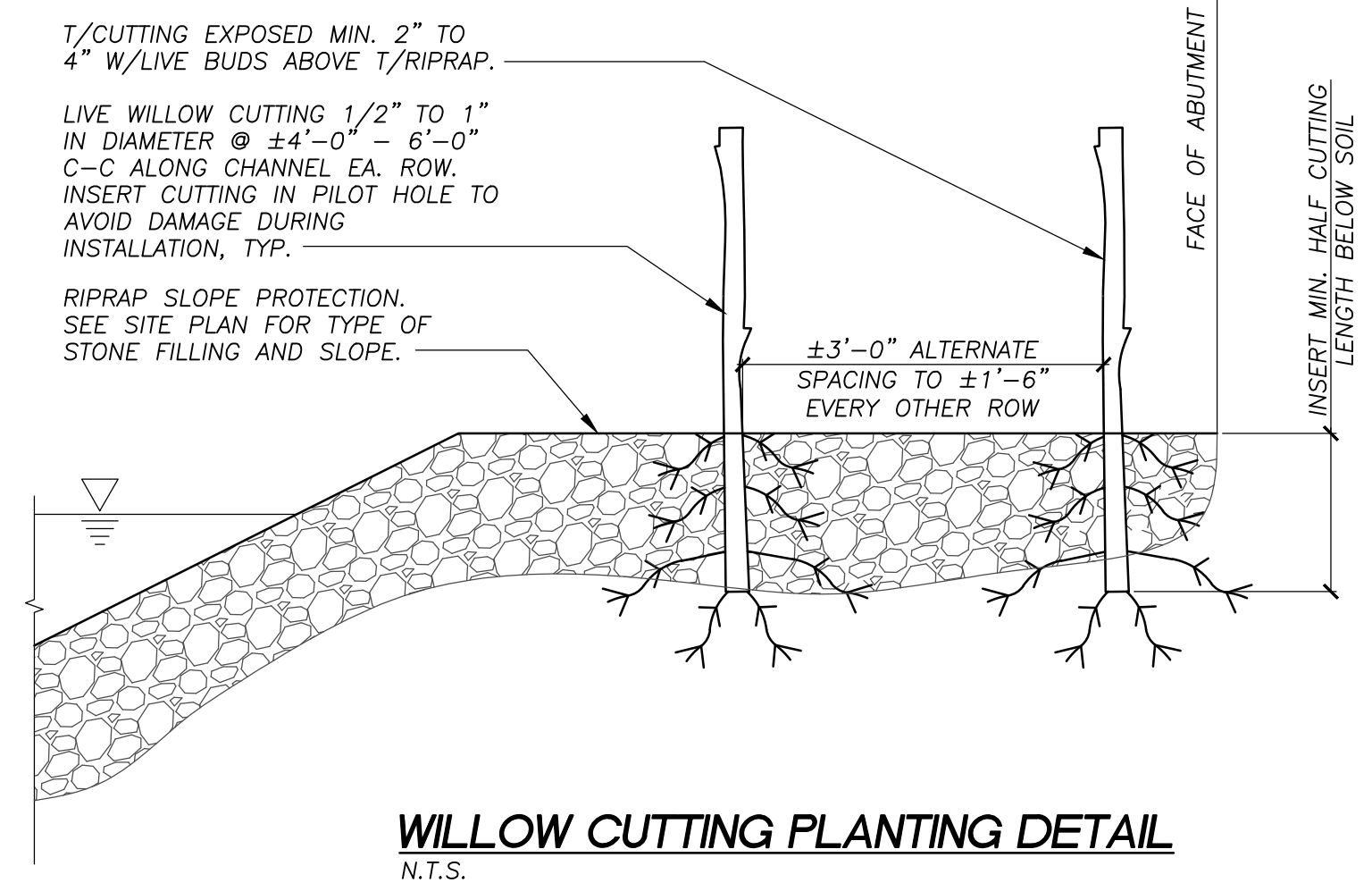
CULVERT PENETRATION DETAIL
N.T.S.



RETAINING WALL LAYOUT SITE PLAN
1"=10'-0"



SEGMENTAL BLOCK WALL SECTION
N.T.S.



WILLOW CUTTING PLANTING DETAIL
N.T.S.

REVISONS	
REV.	DESCRIPTION
0	7/16/19 BID & CONSTRUCTION
1	8/12/19 ADDENDUM No. 1



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DETAILS
DRAWING NO. **C-5** SHT. 5 OF 6
REV. 1